

II P-N junctions Diodes

①

① Introduction

P-N junction is formed when a P-type and a N-type SC are in contact.

* if N-type and P-type are made out of the same material \Rightarrow homojunction.

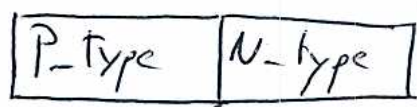
* if N-type and P-type material are different \Rightarrow heterojunction.

* Application = Diode (2 terminal device)

It presents a highly non-linear I-V characteristics and it is often used as a rectifying element.

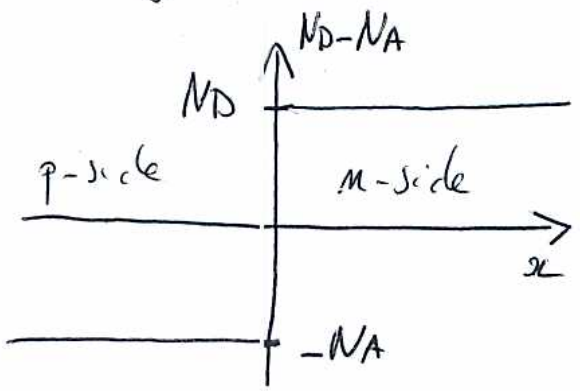
* properties :

P-N junction allows the current flow in one bias direction, but not in the other.

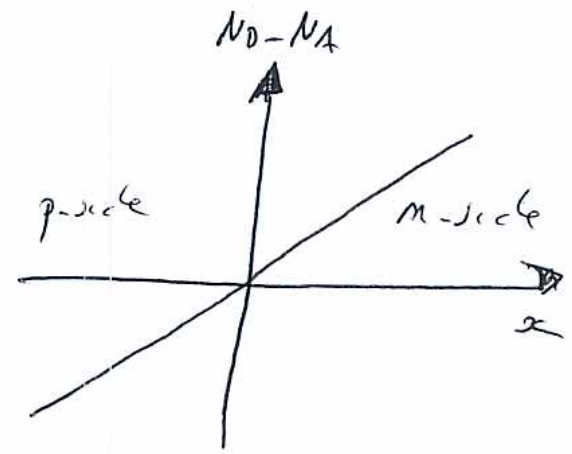


↑
metallurgical junction

P-N junction can be separated into two major categories.



step junction



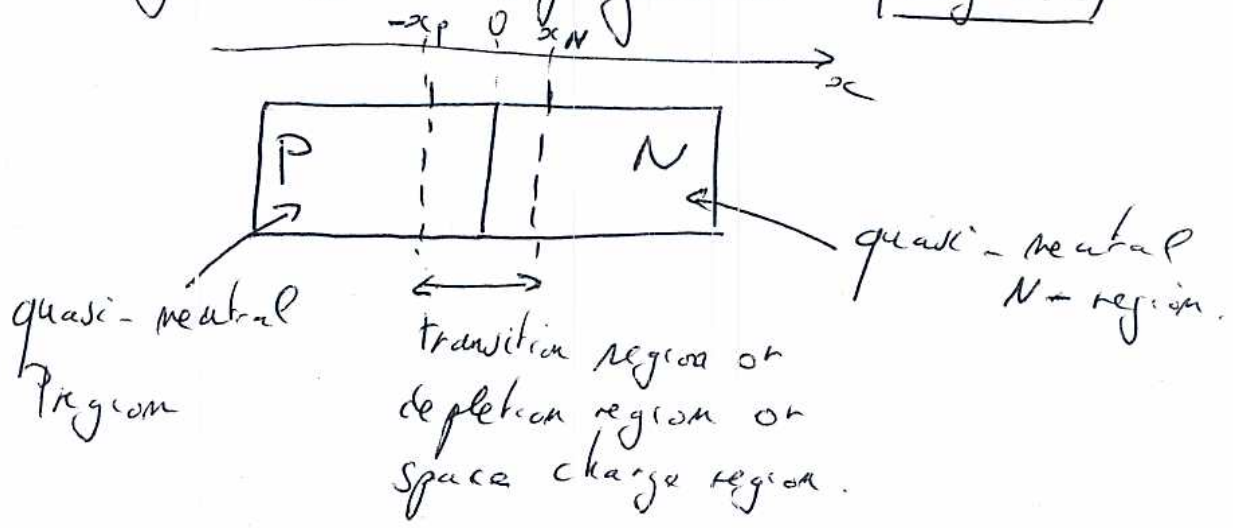
Linearly graded junction

⇒ these are idealized doping profiles see Fig 5.2

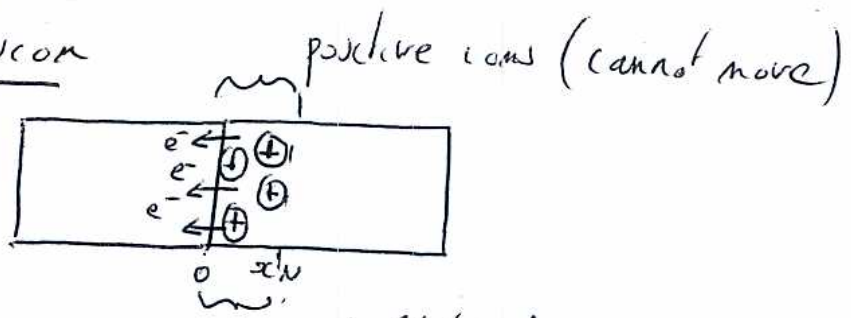
② Built-in potential

① Basic

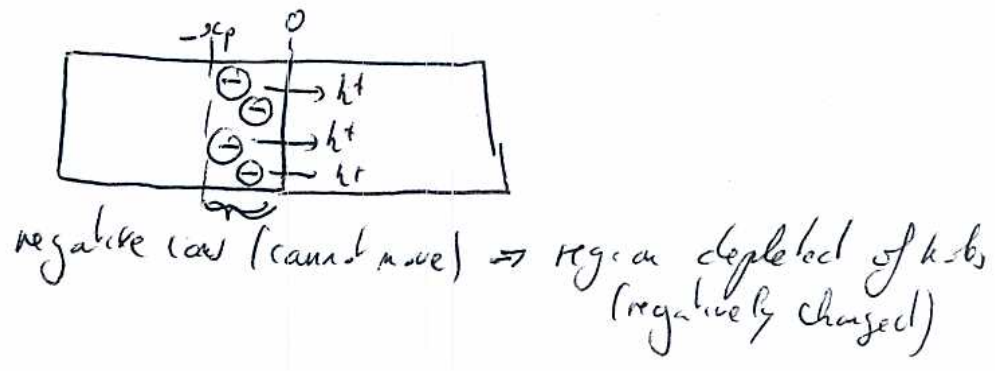
Let us connect 2 pieces (N-type and P-type) and form a PN step junction (Fig 5.5)



• e^- diffusion

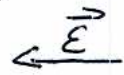


• hole diffusion



Built-in potential

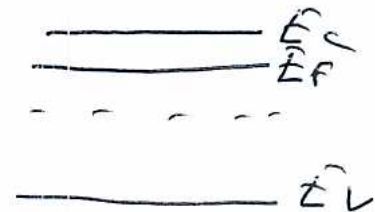
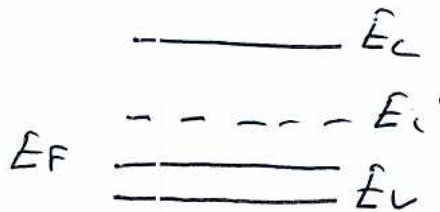
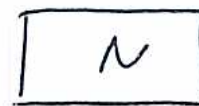
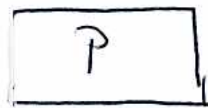
as a result of the diffusion process, a built-in potential, V_0 , is formed at the junction.



Drift $\left\{ \begin{array}{l} \vec{E} \text{ recall the } e^- \text{ back to the N-type region} \\ \vec{E} \text{ " the } h^+ \text{ back to the P-type region.} \end{array} \right.$
 \Rightarrow equilibrium.

(b)* Energy band diagram

Fig 5.3

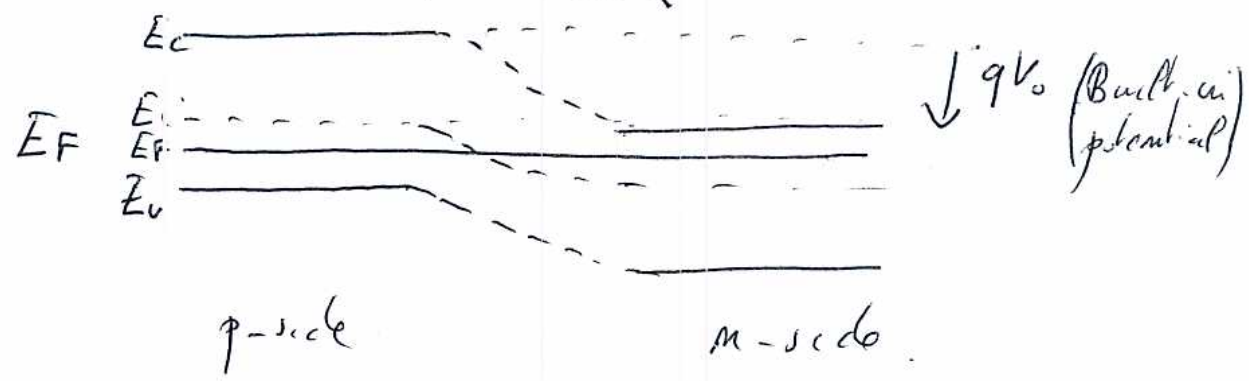


if non degenerate

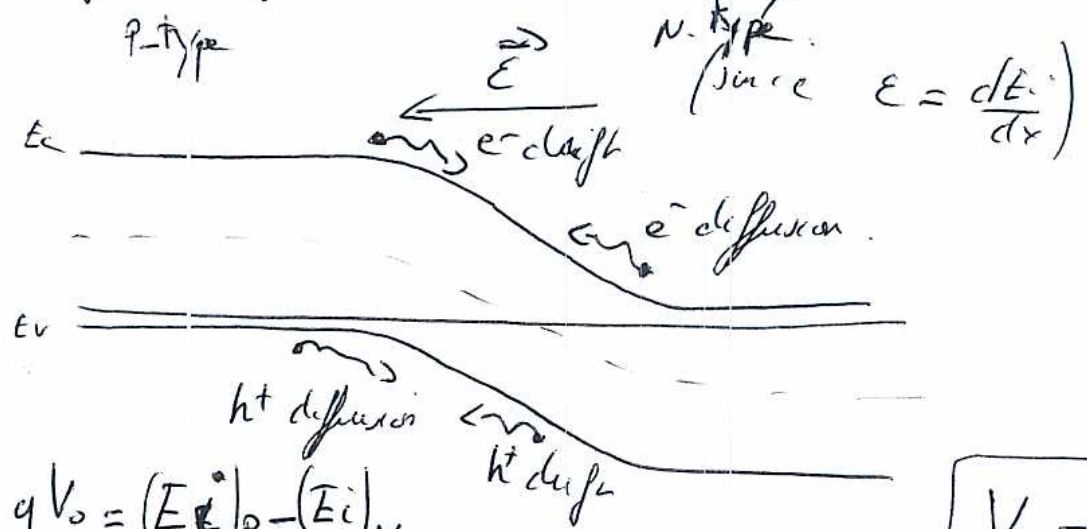
$$E_i - E_F = k_B T \ln\left(\frac{N_A}{n_i}\right)$$

$$E_F - E_i = k_B T \ln\left(\frac{N_D}{n_i}\right)$$

E_F is unique and constant at equilibrium.
 such that transition region



From part 2 of the class we can say that:



$$qV_0 = (E_i)_p - (E_i)_n$$

$$qV_0 = (E_i - E_F)_p + (E_F - E_i)_n$$

$$= k_B T \left(\ln \frac{N_A}{n_i} + \ln \frac{N_D}{n_i} \right)$$

$$V_0 = \frac{k_B T}{q} \ln \frac{N_A N_D}{n_i^2}$$

$$V_0 \equiv V_{bi} \quad (5.10)$$

③ Unbiased junction

what are the charge, potential and electric field variations in the transition region?

we propose to solve the Poisson equation.

~~④ Depletion approximation~~

⇒ Poisson equation is

$$\boxed{-\frac{d^2V(x)}{dx^2} = \frac{\rho}{\epsilon_0 \epsilon_r}} \quad [5.2] / (5.14)$$

or $\boxed{\frac{dE}{dx} = \frac{\rho}{\epsilon_0 \epsilon_r}}$ since $E = -\frac{dV}{dx}$

$\epsilon_r \equiv K$ is dielectric constant

let us call $\epsilon_0 \epsilon_r = \underline{\epsilon_s}$

$$\boxed{\rho_{\text{total charge density}} = -q(n + N_d + N_A - p)}$$

this equation is in practice non-linear since

$$\left[\begin{aligned} n(x) &= n_{n0} e^{\frac{qV(x)}{k_B T}} \\ p(x) &= p_{p0} e^{-\frac{qV(x)}{k_B T}} \end{aligned} \right. \left. \begin{aligned} n, p \text{ depends on } V(x) \\ n_{n0}, p_{p0} \text{ are } e^{-}(h^+) \text{ density} \end{aligned} \right.$$

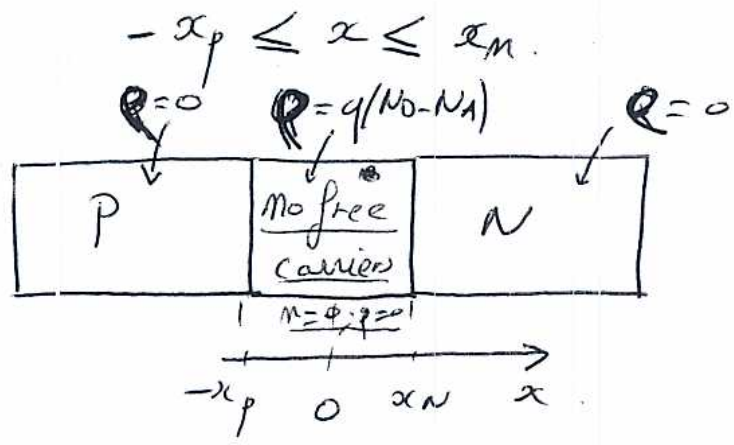
since $E_{i(x)} = E_{i0} - qV(x)$ in the quasi-neutral region N (and P)

Depletion approximation

We cannot solve the Poisson equation analytically, so we use approximation.

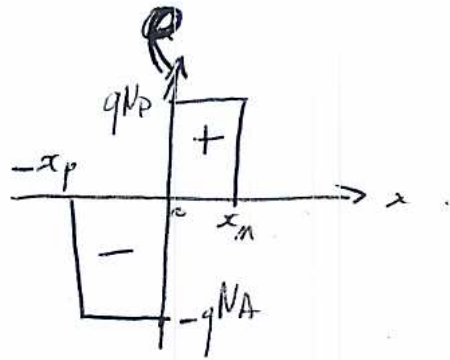
"Depletion approximation" \Rightarrow \vec{E} vanishes outside the depletion region (neutrality) and we ignore the charge due to free carriers in the depletion region.

Depletion approximation.



5.6a

Step junction
Fig 5.66



See also
Fig 5.7
for general
doping profile

Depletion
approximation

$$\begin{cases} N_D \gg n & \text{for } 0 \leq x \leq x_n \\ N_A \gg p & \text{for } -x_p \leq x \leq 0 \end{cases}$$

$$(5.17) \Rightarrow \frac{dE}{dx} = \begin{cases} \frac{qN_D}{\epsilon_s} & \text{for } 0 \leq x \leq x_n \\ -\frac{qN_A}{\epsilon_s} & \text{for } -x_p \leq x \leq 0 \\ 0 & \text{for } x \geq x_n ; x \leq -x_p \end{cases}$$

(b) Solution for Electric field E

→ Solution for $-x_p \leq x \leq 0$.

2 options (for calculations)

$$(i) \frac{dE}{dx} = -\frac{qN_A}{\epsilon_s} \Rightarrow E(x) = -\frac{qN_A}{\epsilon_s}x + a$$

$$E(-x_p) = 0 = +\frac{qN_A x_p}{\epsilon_s} + a \Rightarrow a = -\frac{qN_A x_p}{\epsilon_s}$$

(constant)

↓

$$\Rightarrow \boxed{E(x) = -\frac{q N_A}{\epsilon_s} (x + x_p)} \quad (5.19)$$

$$(ii) \int_0^{E(x)} dE = \int_{-x_p}^x \frac{q N_A}{\epsilon_s} dx \Rightarrow E(x) = -\frac{q N_A}{\epsilon_s} (x + x_p)$$

→ Solution for $0 \leq x \leq x_n$.

$$\frac{dE(x)}{dx} = \frac{q N_D}{\epsilon_s} \quad E(x) = \frac{q N_D}{\epsilon_s} x + a$$

$$E(x_n) = \frac{q N_D}{\epsilon_s} x_n + a = 0 \Rightarrow a = -\frac{q N_D x_n}{\epsilon_s}$$

$$\Rightarrow \boxed{E(x) = \frac{q N_D}{\epsilon_s} (x - x_n)} \quad (5.21)$$

⇒ at $x=0$ it comes $E(x) = -\frac{q N_A x_p}{\epsilon_s} = -\frac{q N_D x_n}{\epsilon_s}$
continuity

$$\Rightarrow \boxed{N_A x_p = N_D x_n} \quad (5.22)$$

charge neutrality condition!

(c) Solution for Electrostatics potential V

$$E = -\frac{dV}{dx} \Rightarrow \frac{dV}{dx} = \begin{cases} \frac{qN_A}{\epsilon_s} (x_p + x) & -x_p \leq x \leq 0 \\ \frac{qN_D}{\epsilon_s} (x_N - x) & 0 \leq x \leq x_p \\ 0 & x \leq -x_p; x \geq x_N \end{cases} \quad (5.23)$$

Let us take the arbitrary reference $V=0$ at $x=-x_p$
 so $V=V_0 (\equiv V_{bi})$ at $x=x_N$ (built-in potential)

\rightarrow for $-x_p \leq x \leq 0$.

$$V(x) = \frac{qN_A}{\epsilon_s} \left(x_p x + \frac{x^2}{2} \right) + a$$

$$V(-x_p) = 0 = -\frac{qN_A}{\epsilon_s} \frac{x_p^2}{2} + a \Rightarrow a = \frac{qN_A}{\epsilon_s} \frac{x_p^2}{2}$$

$$\Rightarrow \boxed{V(x) = \frac{qN_A}{\epsilon_s} \left(x_p x + \frac{x^2}{2} + \frac{x_p^2}{2} \right) = \frac{qN_A}{2\epsilon_s} (x + x_p)^2} \quad (5.26)$$

→ for $0 \leq x \leq x_n$

$$V(x) = \frac{qN_D}{\epsilon_s} \left(x_n x - \frac{x^2}{2} \right) + a$$

$$V(x_n) = V_{bi} = \frac{qN_D}{\epsilon_s} \left(\frac{x_n^2}{2} \right) + a$$

$$\Rightarrow \underline{a} = V_{bi} - \frac{qN_D}{\epsilon_s} \frac{x_n^2}{2}$$

$$\text{So } V(x) = \frac{qN_D}{\epsilon_s} \left(x_n x - \frac{x^2}{2} - \frac{x_n^2}{2} \right) + V_{bi}$$

$$\Rightarrow \boxed{V(x) = -\frac{qN_D}{2\epsilon_s} (x - x_n)^2 + V_{bi}} \quad (5.28)$$

at $x=0$ (continuity)

$$\boxed{\frac{qN_A}{2\epsilon_s} x_p^2 = V_{bi} + \frac{qN_D}{2\epsilon_s} x_n^2} \quad (5.29)$$

(d) ~~same~~ dimension of the transition region

we know ~~the~~ 2 equations (5.29) and (5.22) for x_n, x_p

After substitution, we get.

$$x_n = \sqrt{\frac{2\epsilon_s V_{bi} N_A}{q N_D(N_A+N_D)}} \quad (5.30a)$$

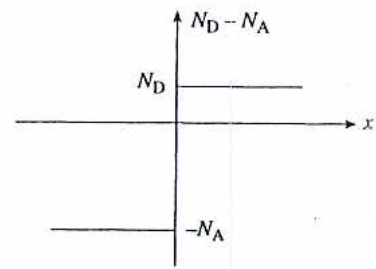
$$x_p = \sqrt{\frac{2\epsilon_s V_{bi} N_D}{q N_A(N_A+N_D)}} \quad (5.30b)$$

$$W = x_n + x_p = \sqrt{\frac{2\epsilon_s (N_A+N_D) V_{bi}}{q N_A N_D}} \quad (5.31)$$

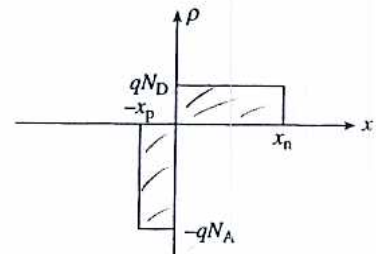
⇒ total width of the depletion region

(c) Summary

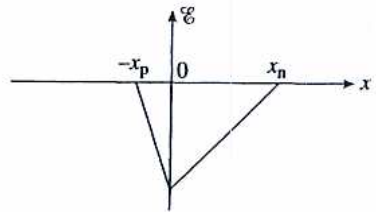
- we know the doping profile N_D-N_A (depletion approx)
- we obtain the built-in potential V_{bi}
- using the depletion approximation we get e
- we calculate E between $-x_n \leq 0 \leq x_p$
- we calculate V between $-x_n \leq 0 \leq x_p$
- we calculate x_n, x_p and $W = x_n + x_p$.



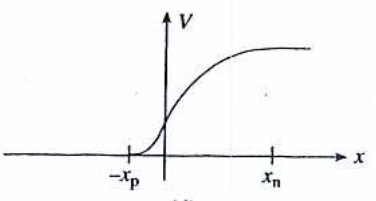
(a)



(b)

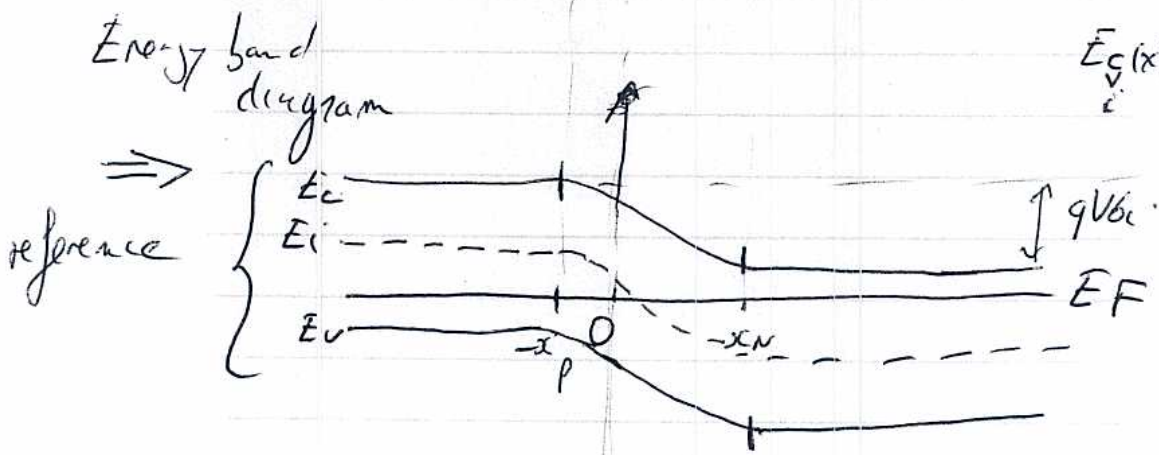


(c)



(d)

Figure 5.9 Step junction solution. Depletion approximation based quantitative solution for the electrostatic variables in a *pn* step junction under equilibrium conditions ($V_A = 0$). (a) Step junction profile, (b) Charge density, (c) electric field, and (d) electrostatic potential as a function of position.



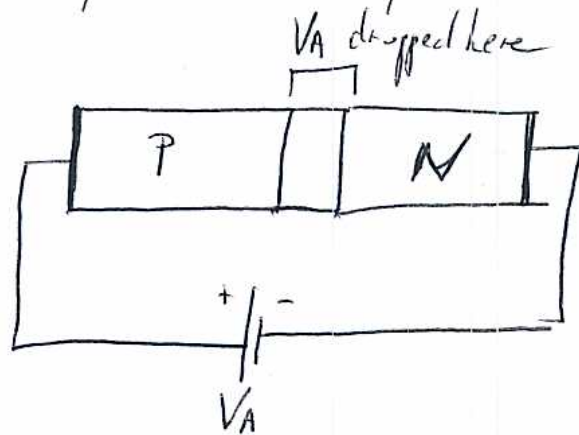
④ Biased junction

① Definition
an external bias, V_A , is now applied to the junction.

Assumption The potential drop across the quasi-neutral regions are negligible ~~small~~.

Therefore the potential drops across the transition region

(See Fig 5.10)



Note: voltage drop of new potential barrier.

$$\boxed{V(x_n) - V(-x_p) = V_{bi} - V_A}$$

{ All the expressions we derived for E, V, x_n, x_p, W
are identical but V_{bi} is now replaced by
 $V_{bi} - V_A$

Equations (5.32) to (5.38)

Example = for w we get

$$W = \left[\frac{2\epsilon_s}{q} \left(\frac{N_A + N_D}{N_A N_D} \right) (V_{bi} - V_A) \right]^{1/2} \quad \underline{5.38}$$

if $V_A > 0 \Rightarrow$ Forward bias.

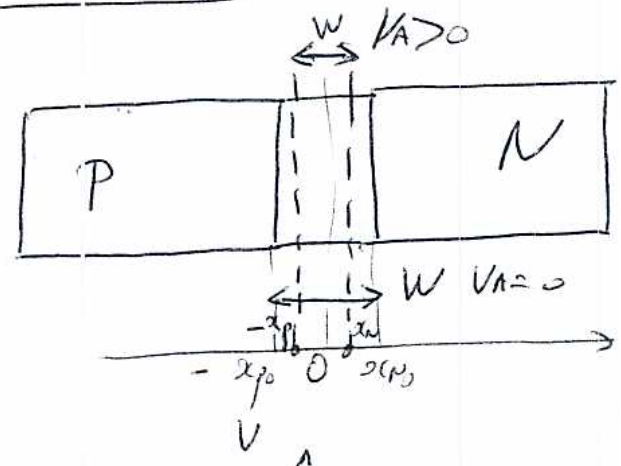
$W \searrow \quad x_n \searrow \quad x_p \searrow$

if $V_A < 0 \Rightarrow$ reverse bias

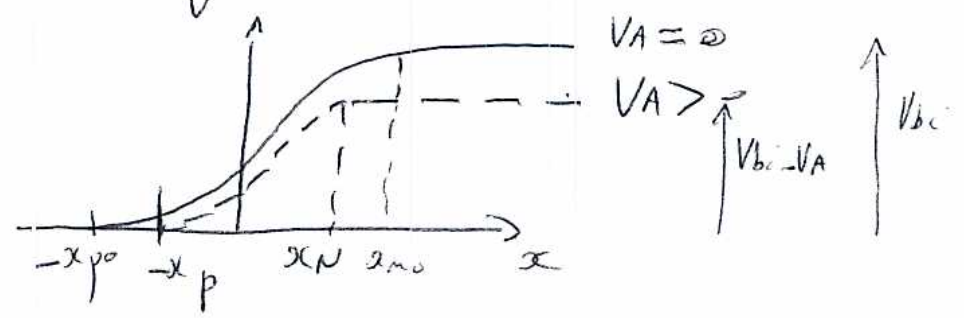
$W \nearrow \quad x_n \nearrow \quad x_p \nearrow$

① Forward bias $V_A > 0$

Fig (5.11)

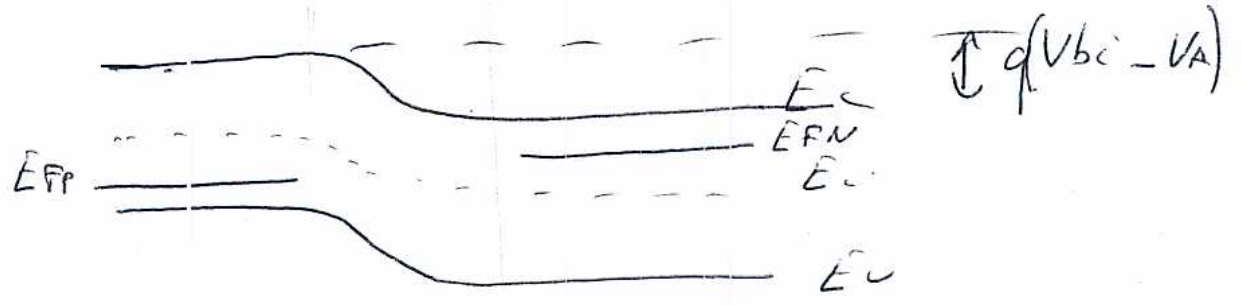


⇒



(Fig 5.14)

⇒



with

$$E_{FN} - E_{FP} = qV_A$$

(E_F is not anymore unique and constant \Rightarrow Non equilibrium)

Diffusion and Electric field/drift forces are no longer equal and opposite sign - Diffusion process > drift process.

⇒ e^- can flow from $N \rightarrow P$
 h^+ can flow from $P \rightarrow N$

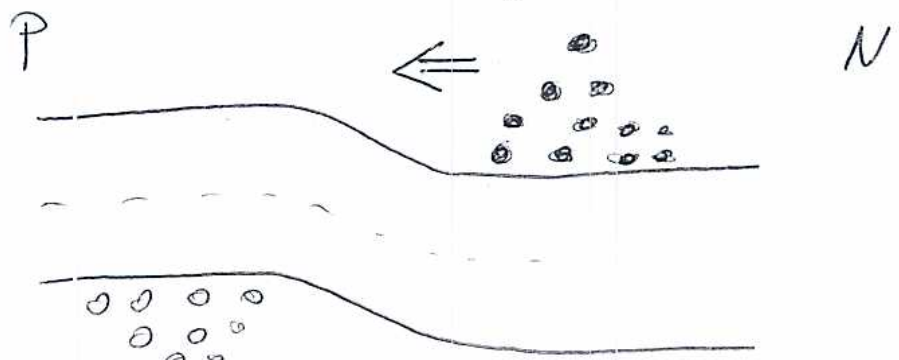
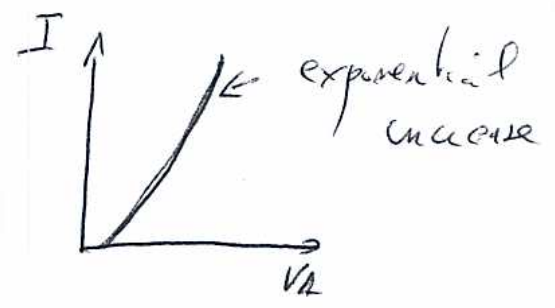
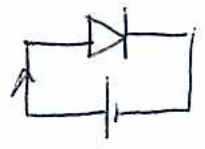
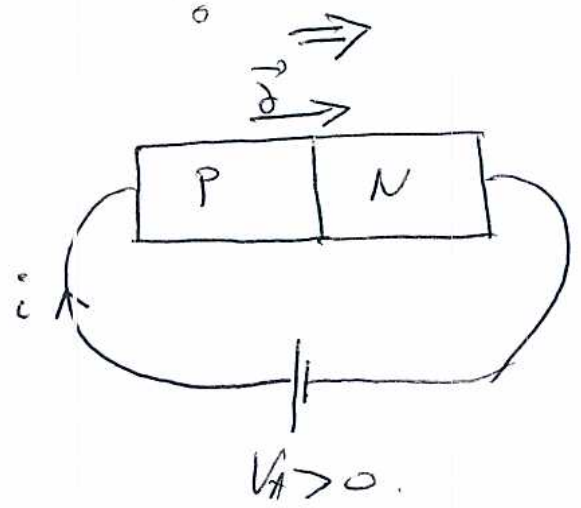


Fig 6.1



© Reverse bias $V_A < 0$

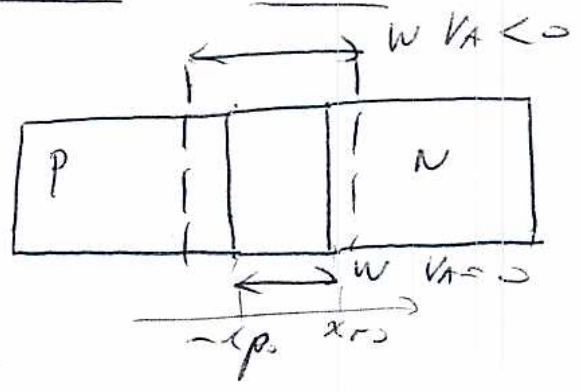
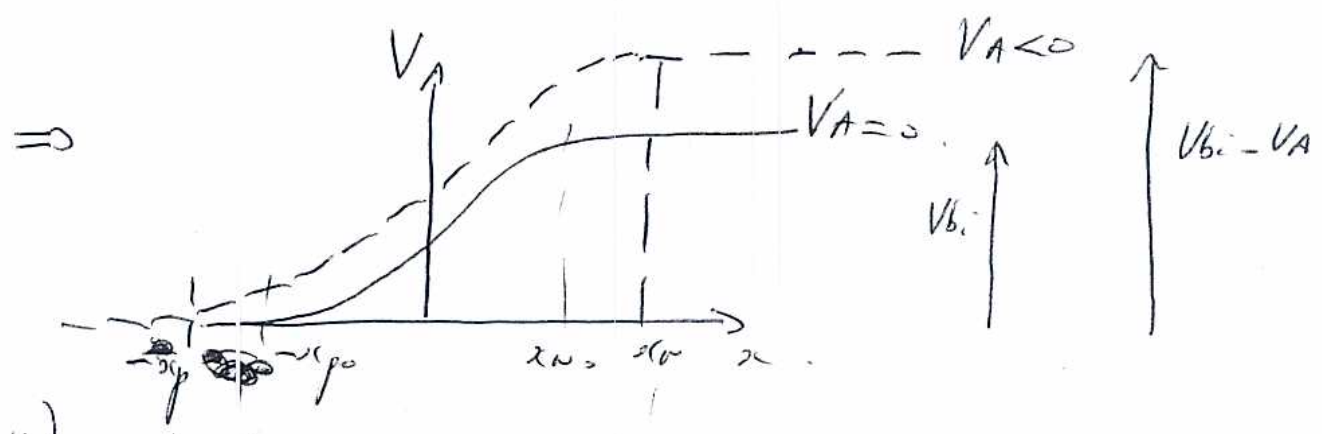
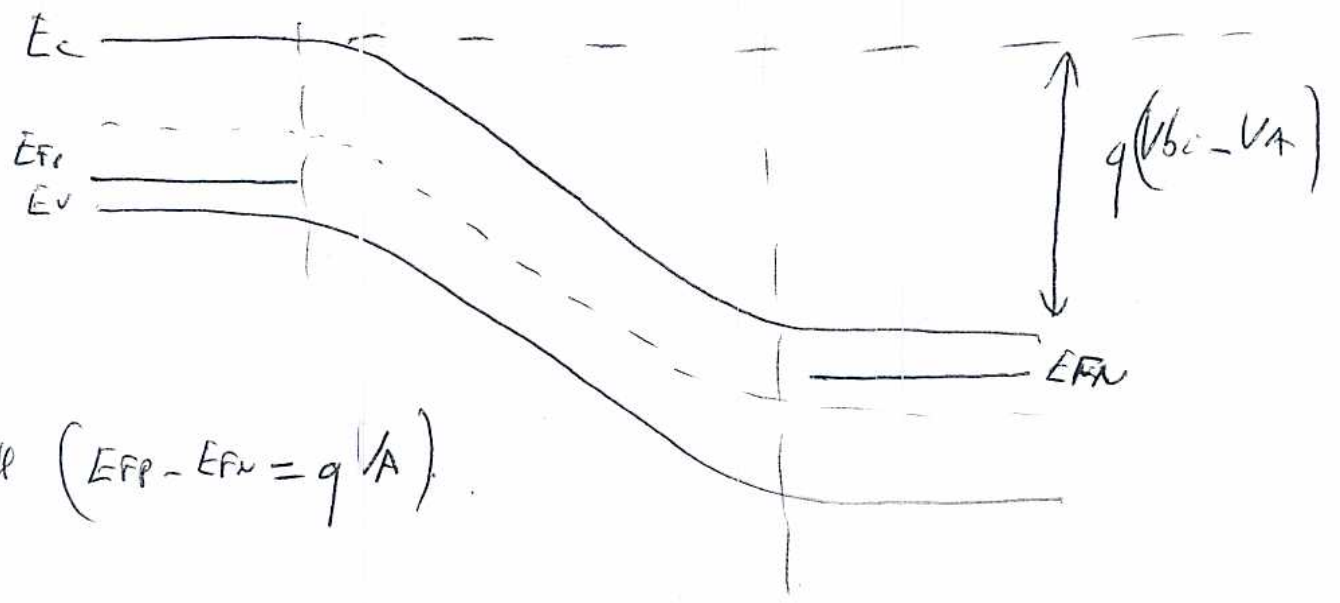


Fig 5.11



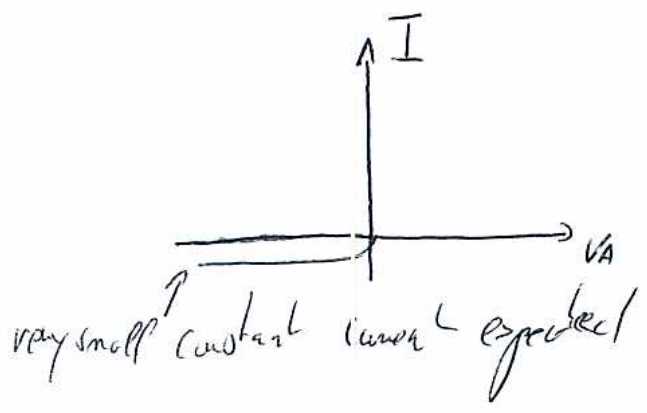
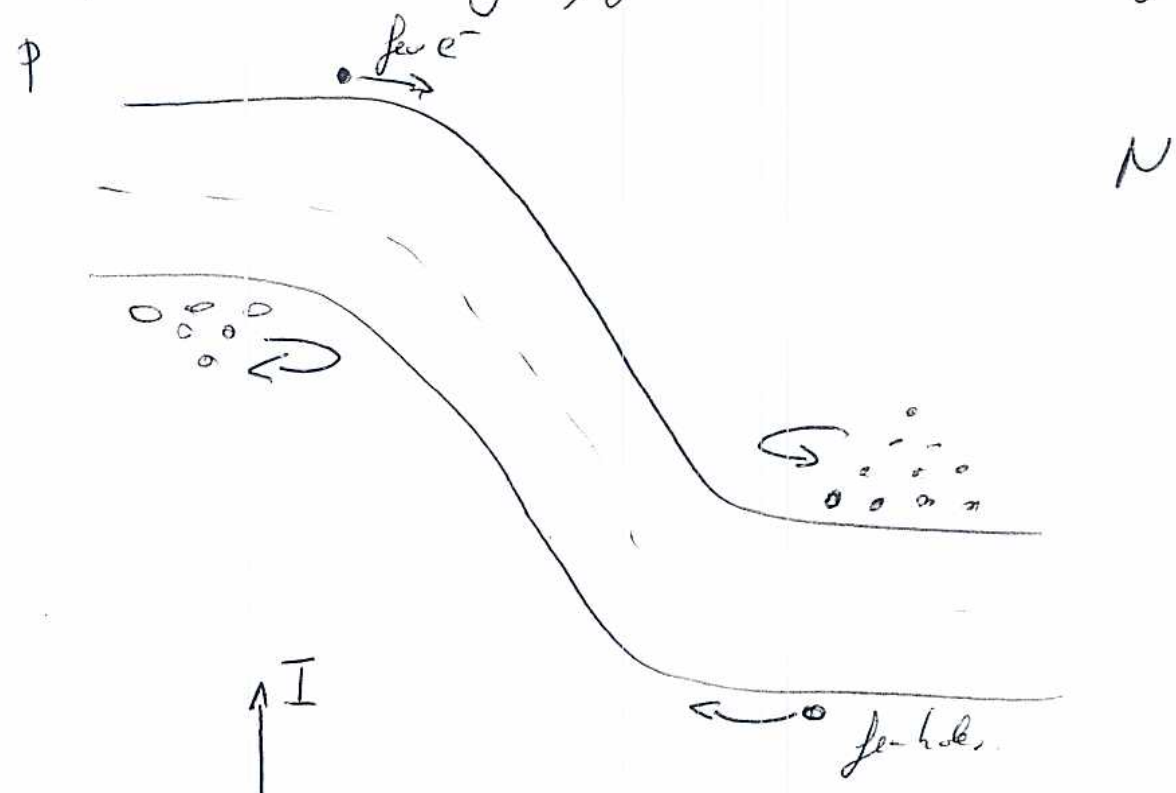
(Fig 5.12)



with $(E_{Fp} - E_{Fn} = qV_A)$

The electric field in the transition region increases and the associated drift current \gg diffusion current

\Rightarrow The magnitude of the resulting net current is very small
(few e^- in the P-region, few holes in the N-region).



P-N junction behaves like a diode rectifying current flow.

5 I-V characteristics

(a) General considerations

So far, what do we know (using the depletion approx.)

P	$\rho = 0$ $E = 0$ $V = 0$	$\rho(x)$ $E(x)$ $V(x)$	$\rho = 0$ $E = 0$ $V = V_{bi} - V_A$	N
		- x_p 0 x_n		

$V_A = \text{applied bias}$

for computing the current, we can make use of

$$I = AJ \quad (A = \text{cross sectional area}) \quad (6.2)$$

$$J = J_n(x) + J_p(x) \quad (6.3)$$

with

$$\begin{cases} J_n = q\mu_n n E + q D_n \frac{dn}{dx} \\ J_p = q\mu_p p E - q D_p \frac{dp}{dx} \end{cases} \quad (6.4)$$

the current J is constant for all position x.

if n and p were available, we are done. However we do not know them (or did not compute them numerically). Let us try to derive an expression for the carrier current ^{first} density J_N in the P-region and J_p in the N-region.

N-side
 (6.6) $J_p = -q D_p \frac{dp}{dx} \quad x \geq x_n \quad (E=0)$

P-side
 $J_n = q D_n \frac{dn}{dx} \quad x \leq -x_p \quad (E=0)$

using the minority carrier diffusion equations.

(6.5) $D_p \frac{d^2 p_n}{dx^2} - \frac{p_n - p_{n0}}{\tau_p} = 0 \quad x \geq x_n$

$D_n \frac{d^2 n_p}{dx^2} - \frac{n_p - n_{p0}}{\tau_n} = 0 \quad x \leq -x_p$

p_n means "density of holes in the N-side"

p_{n0} means "density of holes in the N-side at equilibrium"

Let us try to solve for n_p , J_N $x \leq -x_p$

(6.5a)
$$\left[D_n \frac{d^2 n_p}{dx^2} - \frac{n_p - p_{n0}}{\tau_n} = 0 \right] \quad (-\infty \leq x \leq -x_p)$$

\Rightarrow 2 Boundary conditions are necessary.

(i) $n_p(\infty) = p_{n0} \Rightarrow$ { The diode is infinitely long and we have thermodynamic equilibrium far from the junction.

(ii) $n_p(-x_p) = ?$

Techniques for obtaining this boundary conditions

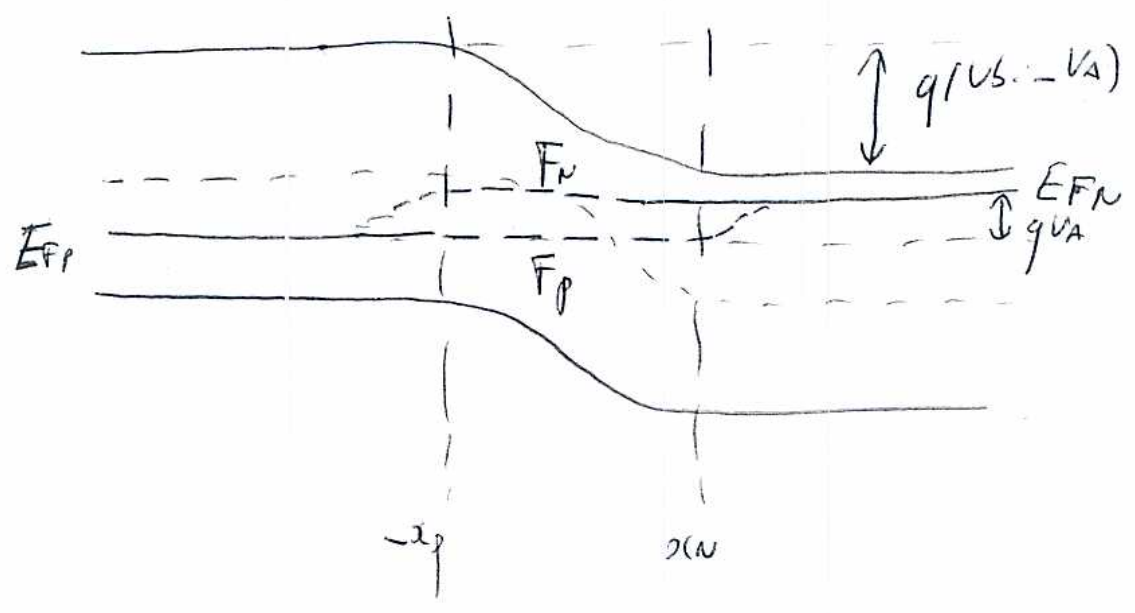
(3.72) we saw that (in equilibrium situation)
$$\begin{cases} n = n_i e^{(F_N - E_i)/k_B T} \\ p = n_i e^{(E_i - F_P)/k_B T} \end{cases} \quad \frac{F_N \text{ and } F_P}{\text{are unref}}$$

From (3.72) we can obtain (6.11)

$$n_p = n_i^2 e^{(F_n - F_p) / k_B T}$$

Valid in the entire device under non equilibrium conditions.

If we look at the following figure (Fig 6.4b)



In the transition region we assume that

$$F_n - F_p = qV_a \quad (\text{monotonic variation})$$

$$\Rightarrow n_p = n_i^2 e^{qV_a / k_B T} \quad -x_p \leq x \leq x_n \quad 6.12$$

at $x = -x_p$

$$n(-x_p) p(-x_p) = n(-x_p) N_A = n_i^2 e^{qV_A/k_B T}$$

$$\Rightarrow n_p(-x_p) = \frac{n_i^2}{N_A} e^{qV_A/k_B T} \quad (6.14)$$

$$AB_0 \left[\frac{n_i^2}{N_A} = n_{p0} \right]$$

we can then solve 6.5

~~$$D_n \frac{d^2 n_p}{dx^2} - \frac{n_p - n_{p0}}{\tau_n} = 0$$~~

$$D_n \frac{d^2 n_p}{dx^2} - \frac{n_p - n_{p0}}{\tau_n} = 0$$

$$\Rightarrow \frac{d^2 n_p}{dx^2} - \frac{1}{L_n^2} (n_p - n_{p0}) = 0$$

$$L_n = \sqrt{D_n \tau_n}$$

Diffusion Length.

$$\Rightarrow n_p(x) = n_{p0} + A \exp\left(-\frac{x}{L_n}\right) + B \exp\left(\frac{x}{L_n}\right)$$

using the Boundary conditions we derived

$$n_p(-\infty) = n_{p0} \Rightarrow A = 0$$

$$n_p(-x_p) = \frac{n_{p0}}{1} e^{qV_A/k_B T} = n_{p0} + B \exp\left(-\frac{x_p}{L_n}\right)$$

$$\Rightarrow B = n_{p0} \left[e^{qV_A/k_B T} - 1 \right] \exp\left(\frac{x_p}{L_n}\right)$$

$$\Rightarrow n_p(x) = n_{p0} + n_{p0} \left[e^{qV_A/k_B T} - 1 \right] \exp\left(\frac{x+x_p}{L_n}\right)$$

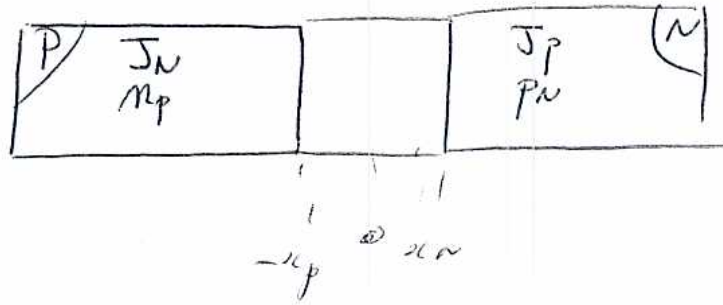
$$6.27a \quad J_N = q D_n \frac{dn}{dx} = q \frac{n_{p0}}{L_n} \left[e^{qV_A/k_B T} - 1 \right] \exp\left(\frac{x+x_p}{L_n}\right) \quad x \leq -x_p$$

Similarly we can obtain

$$p_n(x) = p_{n0} + p_{n0} \left[\exp\left(\frac{qV_A}{k_B T}\right) - 1 \right] \exp\left(-\frac{(x-x_p)}{L_p}\right)$$

$$6.27b \quad J_p = \frac{q D_p p_{n0}}{L_p} \left[e^{qV_A/k_B T} - 1 \right] \exp\left(-\frac{(x-x_p)}{L_p}\right) \quad x > x_p$$

Finally, we have obtained



Remark:

J_p and J_n depends on x .

For example $J_p(x) \rightarrow J \uparrow$. This is due because of the recombination process, here the hole current is transformed into an e^- current. So the total current is independent of x .

to calculate the total current we need to know either J_p in P-type region or J_n in N-type region. These currents involve majority carriers and are very difficult to derive. The total current can be obtained using the ideal diode approximation.

(b) Ideal diode

\Leftrightarrow No G/R in the depletion region.
(Generation/Recombination)

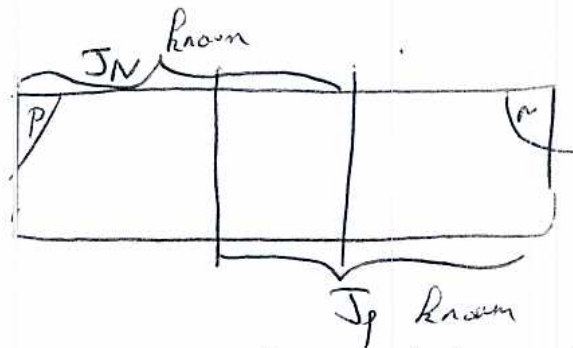
Using continuity equations inside the depletion region:

$$0 = \frac{1}{q} \frac{dJ_n}{dx} - U_n \tag{6.7a}$$

$$0 = \frac{1}{q} \frac{dJ_p}{dx} - U_p \tag{6.7b}$$

if $U_n = U_p = 0 \Rightarrow J_n$ and J_p are constant if $-x_p \leq x \leq x_n$.

So $J_n(-x_p \leq x \leq x_n) = J_n(-x_p)$ (6.8)
 $J_p(-x_p \leq x \leq x_n) = J_p(x_n)$



\Rightarrow we have max overlap between J_n and J_p !

The total current can be obtained by

$$J = J_N(x_p) + J_P(x_n) \quad 6.9$$

Shockley's equation \Rightarrow

$$J = J_0 \left(\exp\left(\frac{qVA}{k_B T}\right) - 1 \right)$$

$$6.29$$

$$I = AJ$$

with

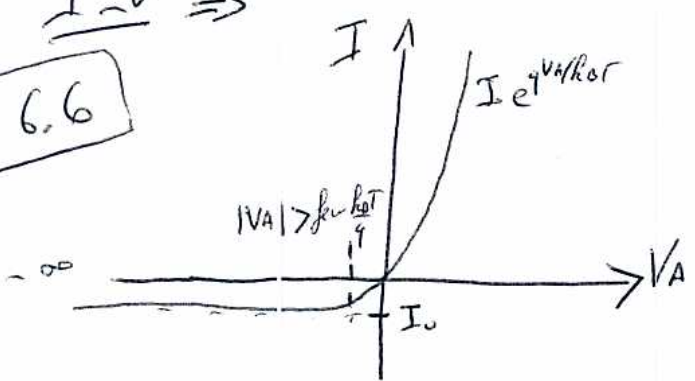
$$J_0 = q \left[\frac{D_n}{L_n} n_{p0} + \frac{D_p}{L_p} p_{n0} \right]$$

$$6.30$$

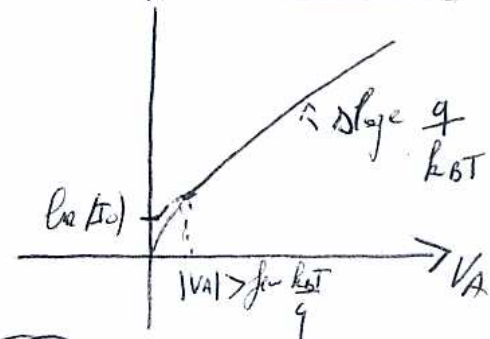
↑ saturation current density

I-V \Rightarrow

Fig 6.6



$\ln(I)$ Semi-log



minority carrier P concentration

Fig 6.8 a

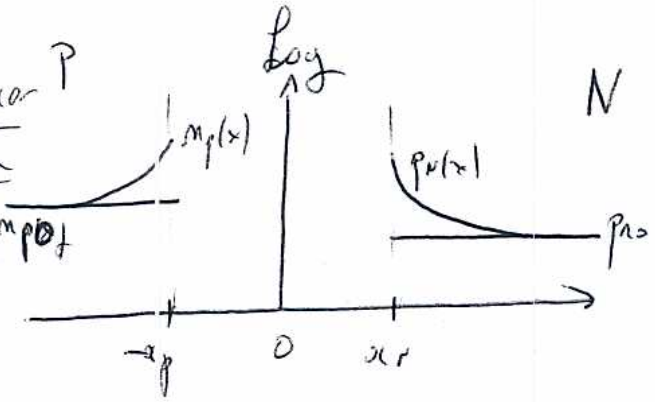
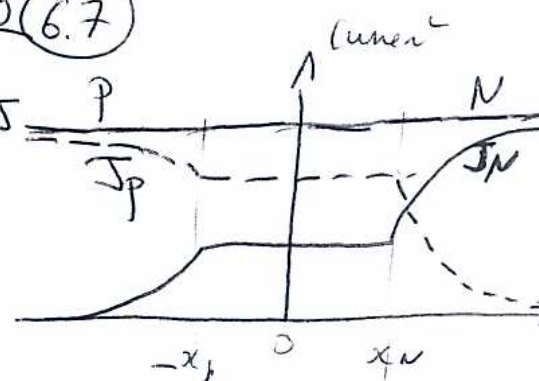


Fig 6.7



$$J = J_n + J_p$$