

I

Camer Jensen 80/80

① 7/7

T=300k

S1

$N_A = 0$

$N_D = 10^{15}/cm^3$

S2

$N_A = 0$

$N_D = 10^5/cm^3$

Also 
$$n = \frac{N_D}{2} + \sqrt{\left(\frac{N_D}{2}\right)^2 + n_i^2} \quad *$$

+1 if justification below are using this formula

For silicon  $n_i = 10^{10}/cm^3$

\* For S1  
 1.  $N_D \gg n_i \Rightarrow$  it is an extrinsic regime.  
 1.  $n \approx N_D$  from (\*)

\* For S2  
 1.  $N_D \ll n_i \Rightarrow$  it is an intrinsic regime.  
 1.  $n \approx n_i$  from (\*)

\* if  $T \uparrow$  in silicon,  $n_i \uparrow$  as well such that for very high T  $n_i > N_D$  and S1 enters in the intrinsic regime ✓ 2.

(2) 10/10

(2)

$$n_i = \sqrt{N_c N_v} e^{-\frac{E_g}{2k_B T}}$$

$n_i$  depends explicitly of the temperature  $T$  with the term  $e^{-\frac{E_g}{2k_B T}}$   
 we will not consider the implicit temperature dependence of  $N_c, N_v, E_g, m_n^*, m_p^*$ .

$$\Rightarrow \ln\left(\frac{n_i}{\sqrt{N_c N_v}}\right) = -\frac{E_g}{2k_B T} \Rightarrow \boxed{T = \frac{-E_g}{2k_B \ln\left(\frac{n_i}{\sqrt{N_c N_v}}\right)}} \quad /4$$

$$n_i = 2 \cdot 10^{13} / \text{cm}^3 \quad (\text{Ge at } 300\text{K})$$

Let us suppose  $k_B T$  even if  $T \neq 300\text{K}$

$$N_{c,v} = (2.51 \times 10^{19}) \left(\frac{m_{n,p}^*}{m_0}\right)^{3/2}$$

For Silicon

$$m_n^* = 1.18 m_0 \quad m_p^* = 0.81 m_0$$

$$E_g = 1.12 \text{ eV} \quad (\text{or } 1.12 \text{ e Joules})$$

$$\boxed{T \approx 463 \text{ K}} \quad /3$$

For GaAs

$$m_n^* = 0.066$$

$$m_p^* = 0.52$$

$$E_g = 1.42 \text{ eV}$$

$$\boxed{T \approx 715 \text{ K}} \quad /3$$

(3)  $E_G^A = 1\text{eV}$        $E_G^B = 2\text{eV}$

$$n_i^{A,B} = \sqrt{N_C^{A,P} N_V^{A,B}} e^{-E_G^{A,B}/2k_B T} \quad /2$$

We suppose  $N_C^A = N_C^B$   
 $N_V^A = N_V^B$

$$\left[ \frac{n_i^A}{n_i^B} \right] = e^{-(E_G^A - E_G^B)/2k_B T} \approx 2.5 \times 10^8 \quad //$$

/4

at  $T=300\text{K}$

Comments:  $n_i$  carrier concentration (intrinsic carrier density) increases exponentially if  $E_G$  decreases. /4

(4) 19/19

(a)  $T=300\text{K}$  n-type  $N_D = 10^{15}/\text{cm}^3$

$$[n \approx N_D = 10^{15}/\text{cm}^3]$$

$$[p = \frac{n_i^2}{N_D} = \frac{(10^{16})^2}{10^{15}} = 10^5/\text{cm}^3] \quad /3$$

(b)  $T=300\text{K}$  p-type  $N_A=10^{16}/\text{cm}^3$

$p \approx N_A = 10^{16}/\text{cm}^3$

$n = \frac{n_i^2}{p} = \frac{(10^{10})^2}{10^{16}} = 10^4/\text{cm}^3$

(c)  $T=300\text{K}$   $N_A=9 \cdot 10^{15}/\text{cm}^3$   $N_D=10^{16}/\text{cm}^3$

$n = \frac{N_D - N_A}{2} + \left[ \left( \frac{N_D - N_A}{2} \right)^2 + n_i^2 \right]^{1/2} = 1.6 \cdot 10^{15}/\text{cm}^3$

$p = \frac{n_i^2}{n} = \frac{(10^{10})^2}{1.6 \cdot 10^{15}} = 6.25 \cdot 10^4/\text{cm}^3$

(d)  $T=450\text{K}$   $N_A=0$   $N_D=10^{16}/\text{cm}^3$

we cannot say  $n=N_D$  since  $p$  may be important here as well.

we use  $n = \frac{N_D}{2} + \left[ \left( \frac{N_D}{2} \right)^2 + n_i^2 \right]^{1/2}$

However, what is  $n_i$  at  $T=450\text{K}$ ?

$n_i = \sqrt{N_c N_v} e^{-E_g/2k_B T}$

$E_g = 1.08\text{eV}$

$m_n^* = 1.18 m_0$

$m_p^* = 0.81 m_0$

$N_c N_v = 4 \left( \frac{m_n^* m_p^*}{m_0} \right)^{3/2} \left( \frac{k_B T}{2\pi \hbar^2} \right)^3$



$$n_i = 4 \cdot 10^{19} / m^3 \Rightarrow \boxed{n_i = 4 \cdot 10^{13} / cm^3} / 2$$

we could also use the formula in the book (directly in  $1/cm^3$ ).

$$n_i = \left( 2.510 \times 10^{19} \left( \frac{m_n^+ m_p^+}{m_0^2} \right)^{3/4} \exp\left( -\frac{E_G}{2kT} \right) \left( \frac{T}{300} \right)^{3/2} \right)$$

Finally  $\boxed{n = 1.14 \cdot 10^{14} / cm^3}$  / 3

and  $\boxed{p = \frac{n_i^2}{n} = 1.4 \cdot 10^{13} / cm^3}$  / 3

5/5  $T = 650K$   $N_A = 0$   $N_D = 10^{15}$

the same  $E_G = 1.015 eV$ .

$$\boxed{n_i \approx 9.1 \cdot 10^{15} / cm^3}$$
 also look at Fig 2.20 / 2

$$\Rightarrow \left\{ \begin{array}{l} n \approx 9.15 \cdot 10^{15} / cm^3 \approx n_i \\ p = \frac{n_i^2}{n} \approx n_i \end{array} \right\} \text{ intrinsic regime} \\ \text{Look at Fig 2.22} / 3$$

5  
6/6 N-type

$$E_c - E_F = 0.2 \text{ eV}$$

$$n \approx N_D = N_c \exp\left(\frac{E_c - E_F}{k_B T}\right) / 3$$

$$\Rightarrow \boxed{N_D = 1.2 \cdot 10^{16} / \text{cm}^3} / 3$$

6  
8/8  $N_D = 2.3 \cdot 10^{17} / \text{cm}^3 \Rightarrow$  N-type - Ge

~~not~~ if non degenerate

$$\left[ \begin{array}{l} n \approx N_D = 2.3 \cdot 10^{17} / \text{cm}^3 \\ p = \frac{n_i^2}{n} = 1.4 \cdot 10^{-5} / \text{cm}^3 \end{array} \right] / 2$$

$$\underline{n_i = 1.8 \cdot 10^6 / \text{cm}^3}$$

$$\begin{array}{l} * \\ \frac{E_c - E_F}{(E_c = 1.42 \text{ eV})} = \frac{E_c - E_i}{\frac{E_g}{2}} + \frac{E_i - E_F}{\frac{k_B T}{e} \ln\left(\frac{n}{n_i}\right)} \approx \underline{0.05 \text{ eV}} / 2 \end{array}$$

The condition  $E_c - E_F > 3k_B T$  is not satisfied !!

$E_F$  is very close to  $E_c \Rightarrow$  SC is degenerate. / 4

2. Consequences (i) ~~the~~ the formula  $m_i^2 = m_p$  is not valid (7)  
 the results previously obtained for  $n$  and  $p$  are questionable.

(ii)  $E_c - E_F$  cannot be approximated by  $\frac{k_B T}{q} \ln \left( \frac{n}{n_i} \right)$ ,  $\Rightarrow E_c - E_F$  is not correct.  
 however  $E_v - E_F$  can be approximated by  $\frac{k_B T}{q} \ln \left( \frac{p}{n_i} \right)$   
 ( $E_F - E_v \gg 3k_B T$ ).

$$\Rightarrow E_c - E_F = \underbrace{E_v - E_F}_{-1.41 eV} + \underbrace{E_c - E_v}_{E_g} = 0.01 eV$$

$E_F$  is even ~~more~~  
 closer to  $E_c$ .

(7) 12/12,  $n_i = 10^{13} / \text{cm}^3$ ,  $n = 2p$ ,  $N_A = 0$ .

$n = \frac{n_i^2}{p} = \frac{2n_i^2}{n} \Rightarrow \boxed{n = \sqrt{2} n_i} = 1.41 \times 10^{13} / \text{cm}^3$

$p = \frac{n_i^2}{\sqrt{2}} = 7.07 \times 10^{12} / \text{cm}^3$

$n = p + Nd \rightarrow Nd = n - p = 7.07 \cdot 10^{12} / \text{cm}^3$  /3

$(E_F - E_i) = k_B T \ln\left(\frac{n}{n_i}\right) = \frac{k_B T}{2} \ln(2) = 1.423 \cdot 10^{-21} \text{ J}$   
~~0.009 eV~~ /3

8/8

indexe

$n_i^{(1)} = n_i \text{ InAs}$        $n_i^{(2)} = n_i \text{ GaAs}$

- (1) for InAs
- (2) for GaAs

$n_i^{(1)} = \sqrt{N_c^{(1)} N_v^{(1)}} e^{-E_g^{(1)} / 2k_B T}$  /2

$n_i^{(2)} = \sqrt{N_c^{(2)} N_v^{(2)}} e^{-E_g^{(2)} / 2k_B T}$

$\frac{n_i^{(1)}}{n_i^{(2)}} = \left( \frac{m_n^{*(1)} m_p^{*(1)}}{m_n^{*(2)} m_p^{*(2)}} \right)^{3/4} e^{-[E_g^{(1)} - E_g^{(2)}] / 2k_B T}$  /4

~~$n_i \text{ InAs} = n_i \text{ GaAs} \left( \frac{m_n^{*(1)} m_p^{*(1)}}{m_n^{*(2)} m_p^{*(2)}} \right)^{3/4} e^{-[E_g^{(1)} - E_g^{(2)}] / 2k_B T}$~~

$\Rightarrow n_i \text{ InAs} = 2.93 \cdot 10^8 \text{ n/GaAs} = 5.86 \cdot 10^{14} / \text{cm}^3$

↑  
see comment on problem (3) /2



# II Carre-kampal 20/20.

(9)

①  
8/8

$$\rho = \frac{1}{(q\mu_n n + q\mu_p p)}$$

ef intrinsik  
 $n = p = n_i$

$$\rho = \frac{1}{q n_i (\mu_n + \mu_p)} \quad /2$$

GaAs  $\Rightarrow$   $\begin{cases} n_i = 1.8 \cdot 10^6 / \text{cm}^3 \\ \mu_n = 8000 \text{ cm}^2 / \text{V.s} \\ \mu_p = 400 \text{ cm}^2 / \text{V.s} \end{cases} \Rightarrow \rho = 413 \cdot 10^6 \Omega \cdot \text{cm} \quad /2$

Si  $\Rightarrow$   $\begin{cases} n_i = 10^{10} / \text{cm}^3 \\ \mu_n = 1360 \text{ cm}^2 / \text{V.s} \\ \mu_p = 460 \text{ cm}^2 / \text{V.s} \end{cases} \Rightarrow \rho = 343 \cdot 10^3 \Omega \cdot \text{cm} \quad /2$

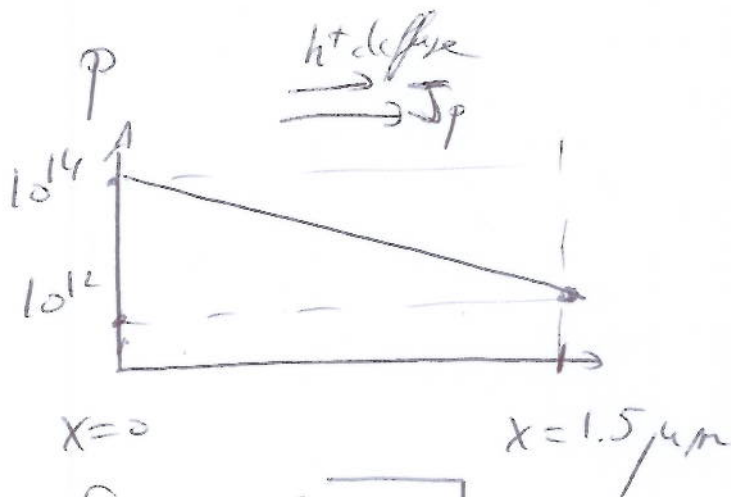
Ge  $\Rightarrow$   $\begin{cases} n_i = 2.0 \cdot 10^{13} / \text{cm}^3 \\ \mu_n = 3900 \text{ cm}^2 / \text{V.s} \\ \mu_p = 1900 \text{ cm}^2 / \text{V.s} \end{cases} \Rightarrow \rho = 54 \Omega \cdot \text{cm} \quad /2$

(10)

(2)  $N_A = 10^{17} / \text{cm}^3$   
 $\mu_p = 317 \text{ cm}^2 / \text{V}\cdot\text{s}$   
 $p \approx N_A$  (p-type)

$$\rho = \frac{1}{q N_A \mu_p} = 0.157 \Omega \cdot \text{cm}$$

(3)  $N_D = 10^{17} / \text{cm}^3$



$$J_p = q D_p \left( \frac{dp}{dx} \right)$$

$$D_p = \frac{k_B T}{q} \mu_p = 8.2 \text{ cm}^2 / \text{s}$$

$$J_p = q D_p \left[ \frac{5.5 \cdot 10^{13}}{1.5 \cdot 10^{-4}} \right] \approx 0.866 \text{ A} / \text{cm}^2$$

Req. The best is to transform everything in S.I

(4)

4/4

$$\mu_m = 8800 \text{ cm}^2/\text{V.s}$$

$$Z_c = \frac{\mu_m m_e^*}{q} = 0.34 \text{ ps} \quad /2$$

mean free path  $v_e = 10^7 \text{ cm/s}$

$$l = v_e Z_c = 34 \text{ mm} \quad /2$$