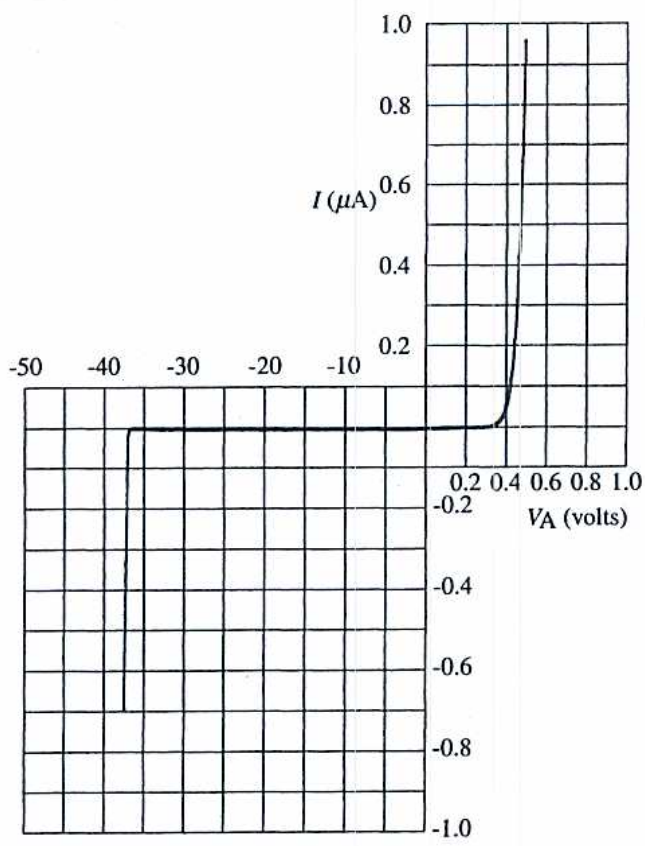


© Deviation from ideality

See Fig. 6.9



**Figure 6.9** Linear plot of the measured  $I$ - $V$  characteristic derived from a commercially available Si pn junction diode maintained at room temperature. The plot permits a coarse evaluation of the diode characteristic. Note the change in voltage scale in going from forward to reverse bias.

in semi-log plot we get Fig 6.1 a and  
Fig 6.10b

Some observations:

reverse Bias  
• For  $V_A < 0$ , the current does not saturate (Fig 6.10b) but continues to increase (still very small) and finally we get a "breakdown" for large reverse bias -

forward Bias  
• For  $V_A > 0$ , ideal characteristics are obtained between  $(0.35 - 0.7V)$ ; for small  $V_A$  the slope (i.e. Fig. 6.10a) is  $\neq$  than  $\frac{q}{k_B T}$  and equal to  $\frac{q}{2k_B T}$ ; for large  $V_A$  ( $V_A \rightarrow V_{bi}$ ) the slope progressively decreases  $\Rightarrow$  "Drope over"

(i) The R-G current

we consider Generation/Recombination in the depletion region (transition region).

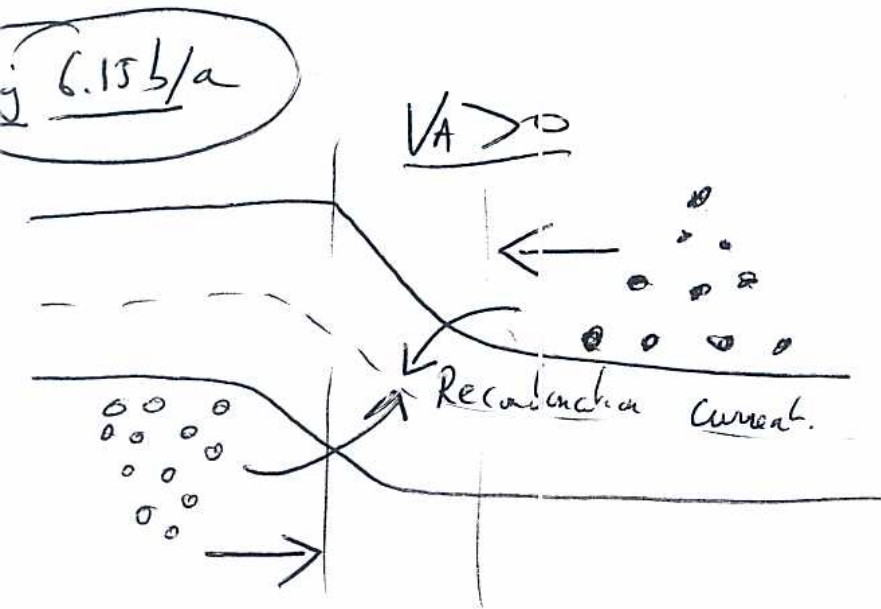
we know that these processes are proportional to

$$n_p - n_i^2$$

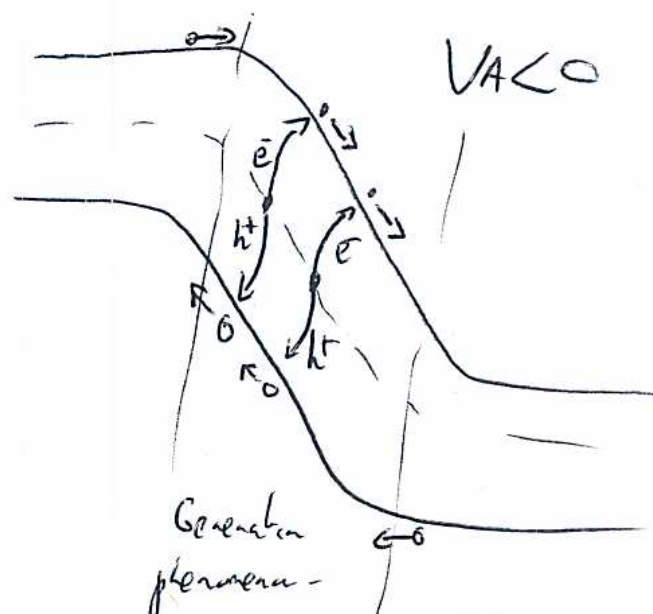
in the forward region we established that

$$n_p = n_i^2 e^{qV_A / k_B T} \quad (6.12)$$

$\left\{ \begin{array}{l} \text{if } V_A > 0 \\ \text{if } V_A < 0 \end{array} \right.$ 
 ~~$n_p > n_i^2$~~   $n_p > n_i^2 \Rightarrow$  Recombination current can be observed in the forward region  
 $n_p < n_i^2 \Rightarrow$  Generation current will be observed in the forward region.



R-G current will decrease ideal current.



R-G current will be added to ideal current.

For the ideal case we said that  $U_n$  and  $U_p = 0$

in 6.7a / 6.7b and then 
$$\begin{cases} J_n(x_p) = J_n(-x_p) \\ J_p(x_n) = J_p(-x_p) \end{cases}$$

The current is constant in the transition region.

here we have 
$$\boxed{\frac{dJ_n}{dx} = -\frac{dJ_p}{dx} = qU}$$
 from continuity equation at the steady states via the intrinsic R/G

$$\Rightarrow \int_{-x_p}^{x_n} \frac{dJ_n}{dx} dx = \int_{-x_p}^{x_n} qU(x) dx$$

$$\Rightarrow J_n(x_n) = J_n(-x_p) + q \int_{-x_p}^{x_n} U(x) dx$$

The net current is

$$J = J_p(x_n) + J_n(x_n) = \underbrace{J_p(x_n) + J_p(-x_p)}_{J_{diff}} + J_G/R$$

$$(6.47) \quad \boxed{J = J_{diff} + J_G/R}$$

using the SRH mechanism (trap assisted) ~~we~~

one can derive an expression for  $J_G/R$

we can obtain expression (6.45)

$$J_{HC} = \frac{q n_i W}{2 \tau_0} \frac{e^{qV_A/k_B T} - 1}{\left( 1 + \frac{V_{bi} - V_A}{k_B T/q} \frac{\sqrt{2n_i \tau_p}}{2 \tau_0} e^{qV_A/2k_B T} \right)}$$

$V_A > 0$  (Forward)

Small bias

The I-V follows  $\left[ \exp\left(\frac{qV_A}{2k_B T}\right) \right]^{Law}$

Characteristics of a recombination dominated current

Large bias

The I-V follows  $\left[ \exp\left(\frac{qV_A}{k_B T}\right) \right]^{Law} \Rightarrow$

Diffusion current takes over and completely overshadows the Recombination current

$V_A < 0$

$J_{R/G}$  is added to  $J_{diff}$ .

So the current keeps increasing (slowly) with  $V_A \searrow$

(ii) Junction breakdown

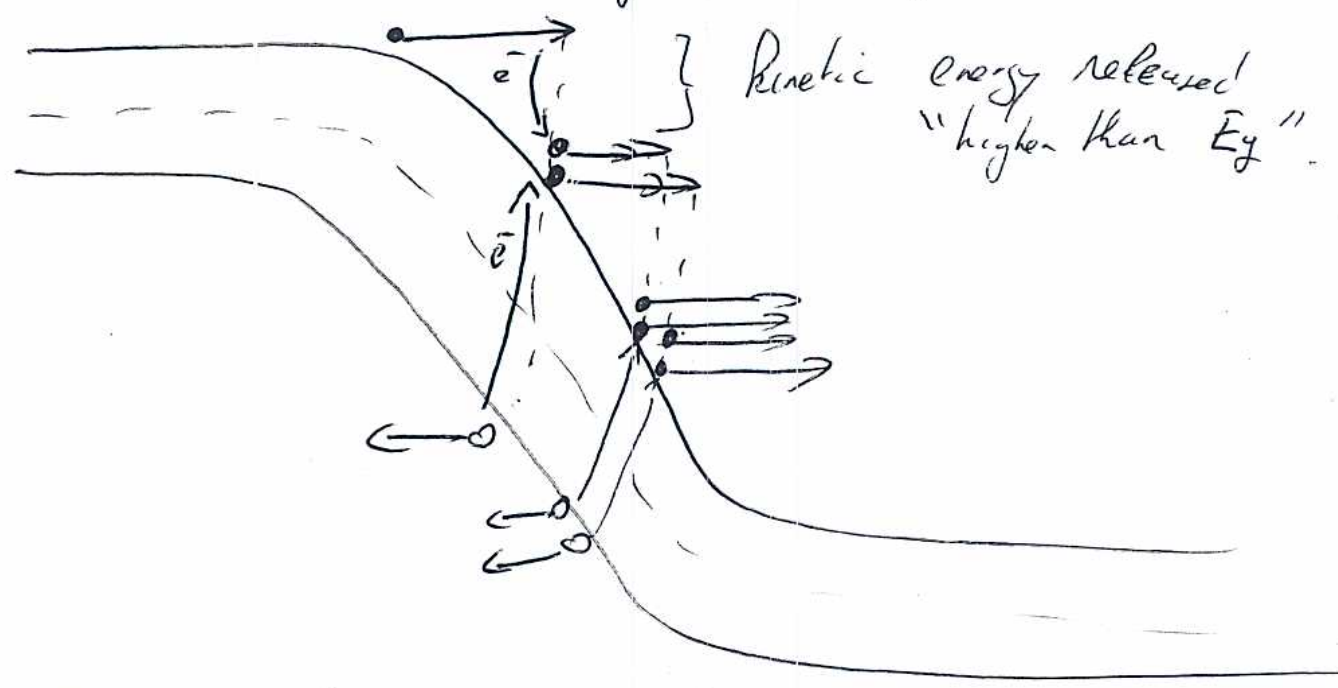
if  $V_A < 0$  strongly reversed biased,  $\vec{E}$  near the metallurgical junction can reach high values. Carriers accelerated in that field can accumulate enough kinetic energy that they can, through a collision process, generate  $e^-h^+$  pairs through "impact ionization".

Impact ionization :

When an  $e^-$  is accelerated to high electric field, its kinetic energy can be equal or larger than the bandgap  $E_g$ . That energy can be released through a collision event, while creating an  $e^-/h^+$  pair. So instead of having one  $e^-$  at high energy,

we get 2 free  $e^- + 1$  hole. We call it  
 generation "by impact ionization"  
 $\Rightarrow$  avalanche multiplication phenomenon.

Fig 6.12



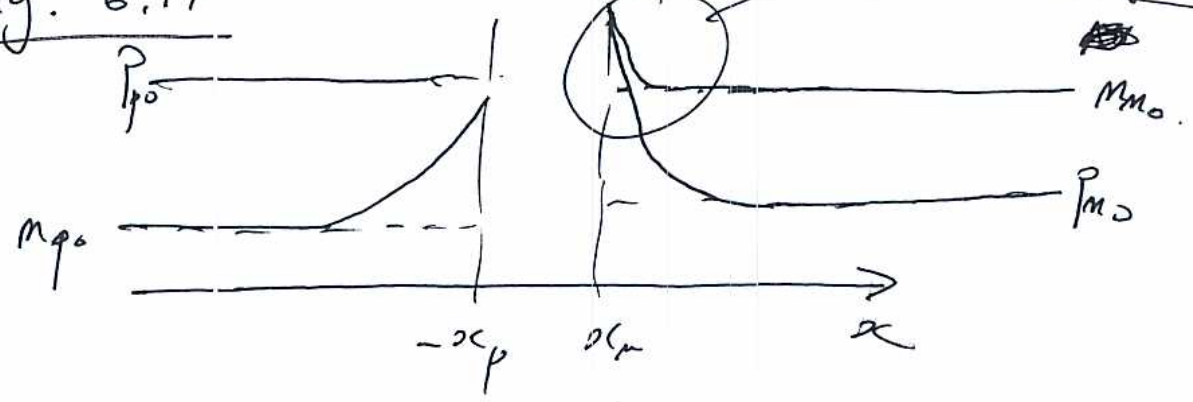
In the P-N junction a sudden increase of current is observed  $\Rightarrow$  breakdown.

(iii) high-level injection

If  $V_A \rightarrow V_{bi}$  the ideal diode equation begins to fail. Indeed the low-level injection of  $h^+$  from  $N \rightarrow P$  or  $e^-$  for  $P \rightarrow N$  is not valid anymore.

Sec Fig. 6.17

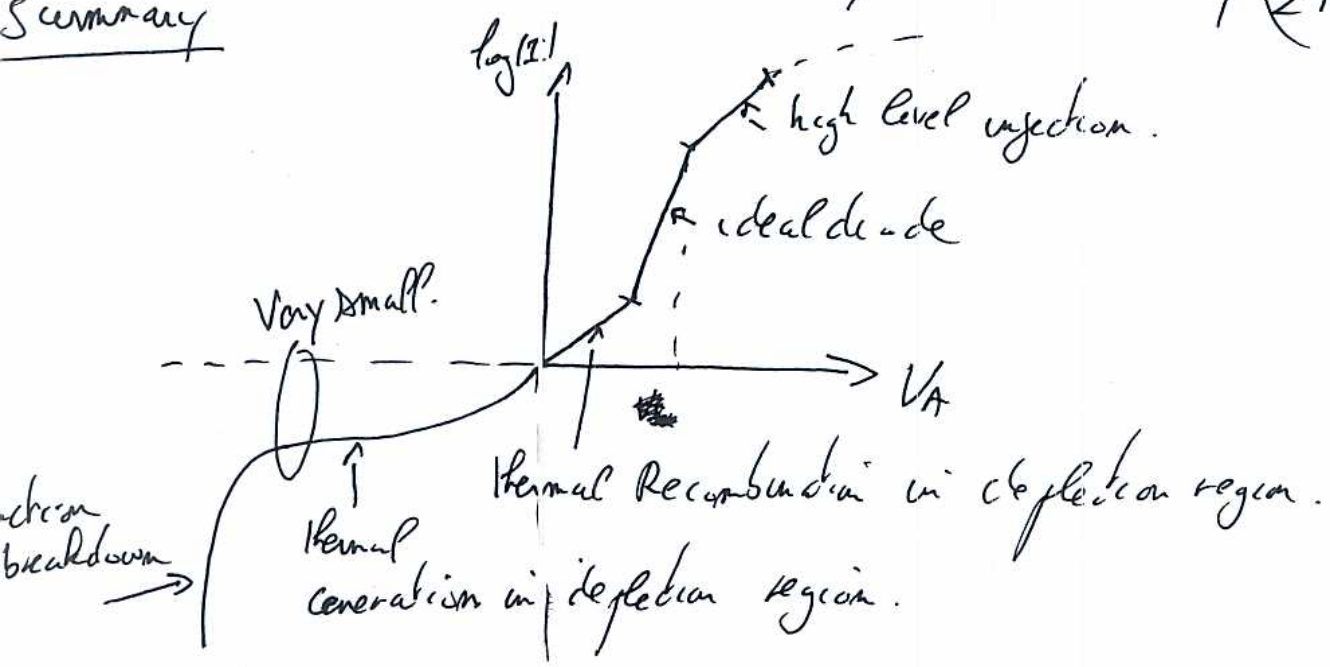
(P)



(N)

The new current will vary  $\sim$  as  $\exp\left(\frac{q}{2k_B T}\right)$

Summary

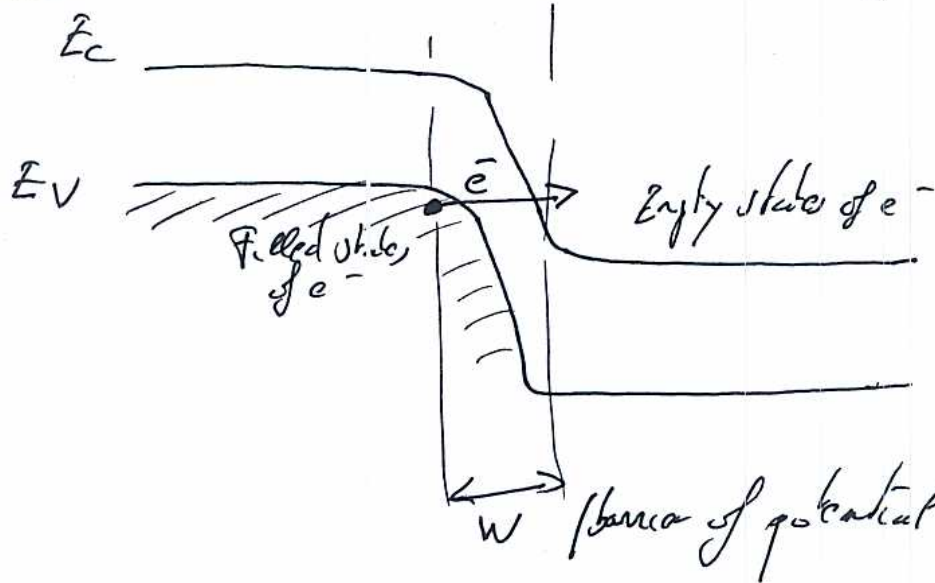


(d) Zener diodes

if n-type and p-type are heavily doped, the width of the transition region is very small;  $\Rightarrow$  quantum tunneling appears in reverse-bias regime.



Fig 6.14



$e^-$  can directly tunnel from P-type valence band to N-type conduction band.


$\Rightarrow$  equivalent to 

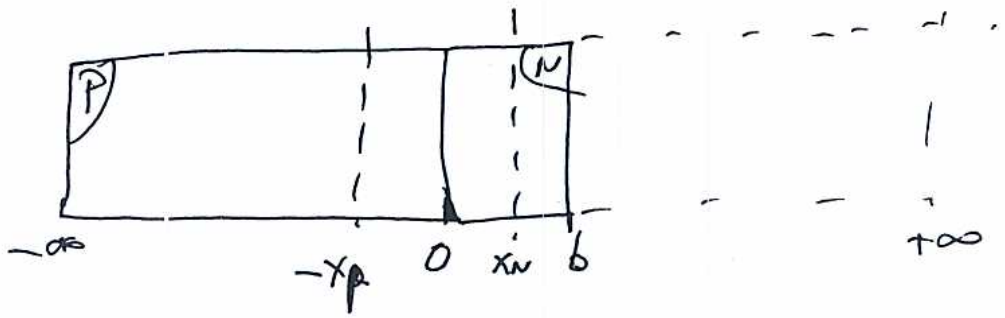
Fig 6.13

These diodes are called "Zener diodes" when the voltage breakdown can be accurately controlled while adjusting the impurity concentration. Zener diodes are then used as voltage reference.

(e) Narrow-base diodes

previously, we assumed that the length of the P and N regions  $\gg$  diffusion length of the minority carriers ( $L_p, L_n$ ).

The term (sharp-base) or (narrow-base) comes from bipolar transistors that consist in 2 P-N junctions PNP or NPN and the central region is called 'base'.



The previous assumption for calculating the minority carriers in the N region  $p_n(x \rightarrow +\infty) = p_{n0}$  must be replaced by  $p_n(b) = p_{n0}$ .

Also  $\rightarrow$  the minority holes will not be able to recombine in the narrow base ( $b \ll L_p$ )  $\Rightarrow J_p$  is then constant  $0 \leq x \leq b$ .

between  $a \leq x \leq b$   $J_p = -q D_p \frac{dp}{dx} \Rightarrow \boxed{p(x) = -\frac{J_p x}{q D_p} + B}$   $p(x)$  is linear

at  $x = x_m$  }  $p(x_m) = p_{m0} \exp\left(\frac{q V_A}{k_B T}\right)$   
 we know that

$\Rightarrow B = p_{m0} \exp\left(\frac{q V_A}{k_B T}\right) + \frac{J_p x_m}{q D_p}$

$\Rightarrow p(x) = -\frac{J_p}{q D_p} (x - x_m) + p_{m0} \exp\left(\frac{q V_A}{k_B T}\right)$

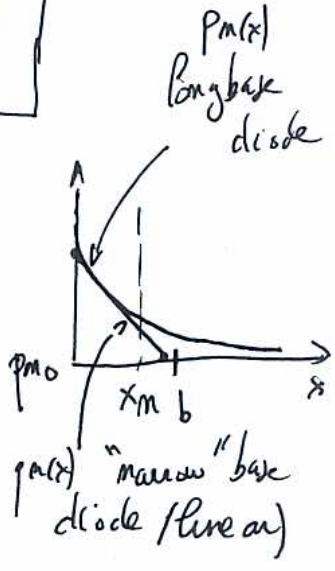
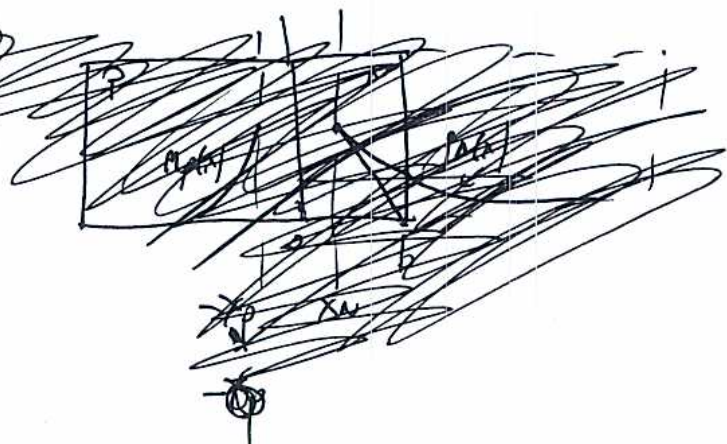
at  $x = b$

$p(b) = -\frac{J_p}{q D_p} (b - x_m) + p_{m0} \exp\left(\frac{q V_A}{k_B T}\right) = p_{m0}$

$\Rightarrow \boxed{J_p = \frac{q D_p p_{m0}}{b - x_m} \left[ \exp\left(\frac{q V_A}{k_B T}\right) - 1 \right]}$

equation equivalent to  
 (6.68)  
 (6.69)  
 matching case  
 6.71a / 6.72a  
 6.73  
 and explanation below.

~~Summary~~



# ⑥ P-N Junction Capacitance.

So far, we considered steady state characteristics, however, it is also important to know how quickly the device can adjust to a new bias condition.

Capacitance calculations will help to estimate this "time response" of the device.

• Capacitance is a measure of charge stored per unit change of voltage.

⇒ this means if capacitance is large, more charge must be moved in or out, so that for a fixed current more time is needed to complete the process.

In P-N junctions, two major capacitance:

(a) Capacitance associated with the charge which must be moved in or out of the depletion region.

⇒ depletion capacitance.

(b) "diffusion capacitance" under forward bias due to minority carriers.

(a) Depletion capacitance

we know that 
$$x_p = \sqrt{\frac{2 \epsilon N_d (V_{bi} - V_A)}{q N_A (N_A + N_d)}}$$

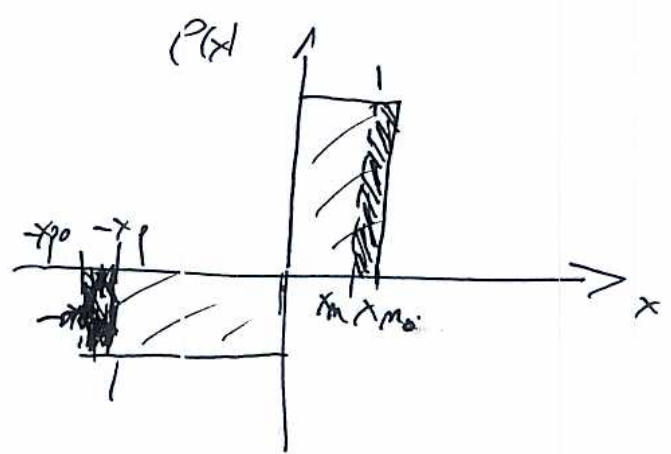
$$x_n = \sqrt{\frac{2 \epsilon N_A (V_{bi} - V_A)}{q N_D (N_A + N_D)}}$$

The charge of the fixed, ionized impurities in each

depletion region is:  
(absolute value)

$$Q = A q N_d x_n = A q N_A x_p$$

A = cross section of the device.



$x_{m0}, -x_{p0} \Rightarrow V_A$   
 $x_m, -x_p \Rightarrow V_A + \Delta V_A$   
 $\Delta V_A > 0$

Capacitance is  $C_T = \left| \frac{dQ}{dV_A} \right| = AqNd \left| \frac{dx_m}{dV_A} \right|$

after calculation  $\Rightarrow$

$$C_T = \frac{A \epsilon}{x_m + x_p} = \frac{A \epsilon}{w} \quad (x_m + x_p = w)$$

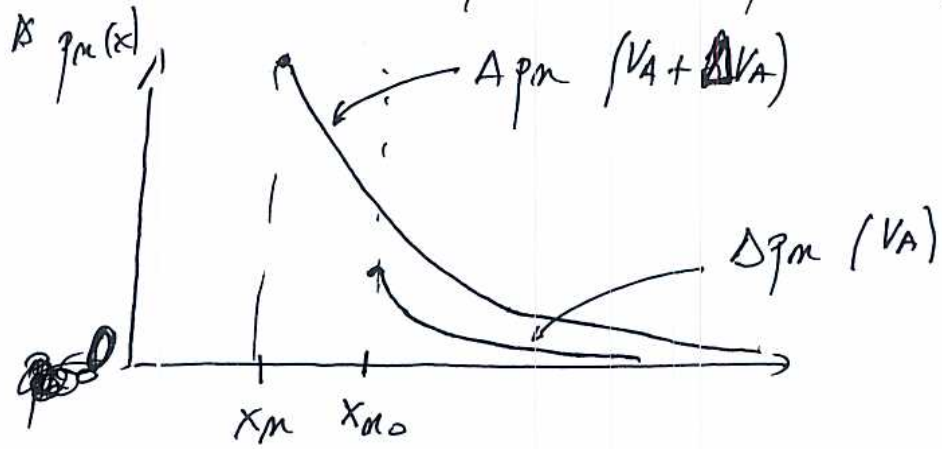
$\Rightarrow$  it is the capacitance of parallel plate capacitor with a dielectric of permittivity  $\epsilon$ .

⑧ Diffusion capacitance

Let us look at the hole concentration in the n-t-type region.

$$p_n(x) = p_{n0} + p_{n0} \left[ \exp\left(\frac{qV_A}{k_B T}\right) - 1 \right] e^{-\frac{x-x_0}{L_p}}$$

Excess concentration is  $\Delta p_m(x) = p_m(x) - p_{m0}$ .



$$Q = q \int_{x_n}^{+\infty} \Delta p_m(x) = q p_{m0} \left( \exp\left(\frac{qV_A}{k_B T}\right) - 1 \right) * L_p$$

diffusion capacitance for p-side

$$C_{Dp} = \frac{dQ}{dV_A} = \frac{q^2 L_p}{k_B T} p_{m0} \exp\left(\frac{qV_A}{k_B T}\right)$$

Also  $C_{Dp} = \frac{q \tau_p}{k_B T} J_p(x_n)$

Similarly  $C_{Dn} = \frac{q \tau_n}{k_B T} J_n(-x_p)$

$$C_D = C_{Dp} + C_{Dn} = \frac{q}{k_B T} [ \tau_p J_p(x_n) + \tau_n J_n(-x_p) ]$$