



# Implementation of the Oriented-Eddy Collision Turbulence Model in OpenFoam

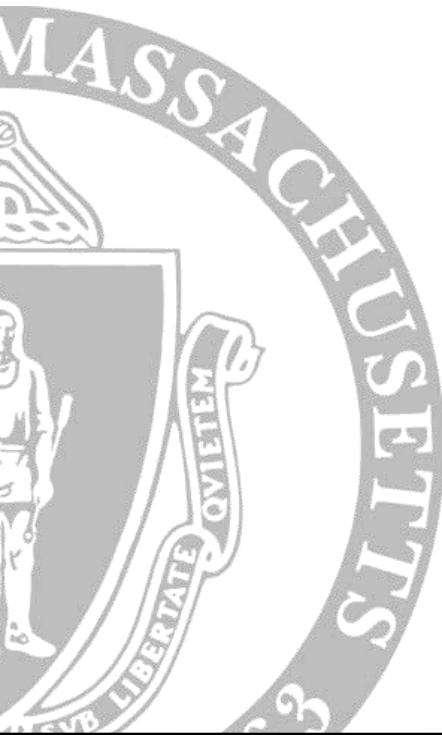
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## Goal: Develop a New Turbulence Model

### **Navy Requirements**

- Easy for others to test.
- Easy for others to adopt.
- Easy to test real world applications.



### **Our Requirements**

- Solve coupled tensor PDE's.
- Mixed BCs.
- Handle arbitrary numbers of equations.

# Why OpenFoam?

## ■ Advantages over commercial code

- Free, open source, parallel
- Users can inspect, alter, expand on the source code.

```
tmp<fvScalarMatrix> kEqn
(
    fvm::ddt(kINT)
    - fvm::laplacian(dEff(), kINT)
    + fvm::SuSp((alpha*nu()*qsq + tauR), kINT)
    ==
    - fvc::div(phi_., kINT)
    + (Ptmp && (Ri)StarINT*kINT))
    - A
    + M
);
```

## ■ Advantages over in house code development

- Many numerical methods, operators, utilities already implemented and tested

## ■ Large, user-driven support community

- Interact with other OpenFOAM users.
- Get help from CFD experts.



# Why OpenFoam?

## Advantages

- Free,
- Users can write their own code.

## Advantages

- Many users have already used it.

## Large, user-driven support community

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    + M
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```

New Thread	
Threads in Forum : OpenFOAM	
Thread / Thread Starter	
 sHM and cyclicGgi FabOr	
 Simple hardcoding boundary conditions Noggin	
 How to modify discrete scheme crammer008	

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    - A
    + M
);
```

## ■ Advantages

- Many already

## ■ Large,

- Inter
- Get h



## Prior Experience:

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### **In House Codes**

- UNS3D: Moving unstructured staggered mesh code for two-phase incompressible flows
- Stag++: Cartesian staggered mesh for DNS/LES of incompressible turbulence.

### **Fluent**

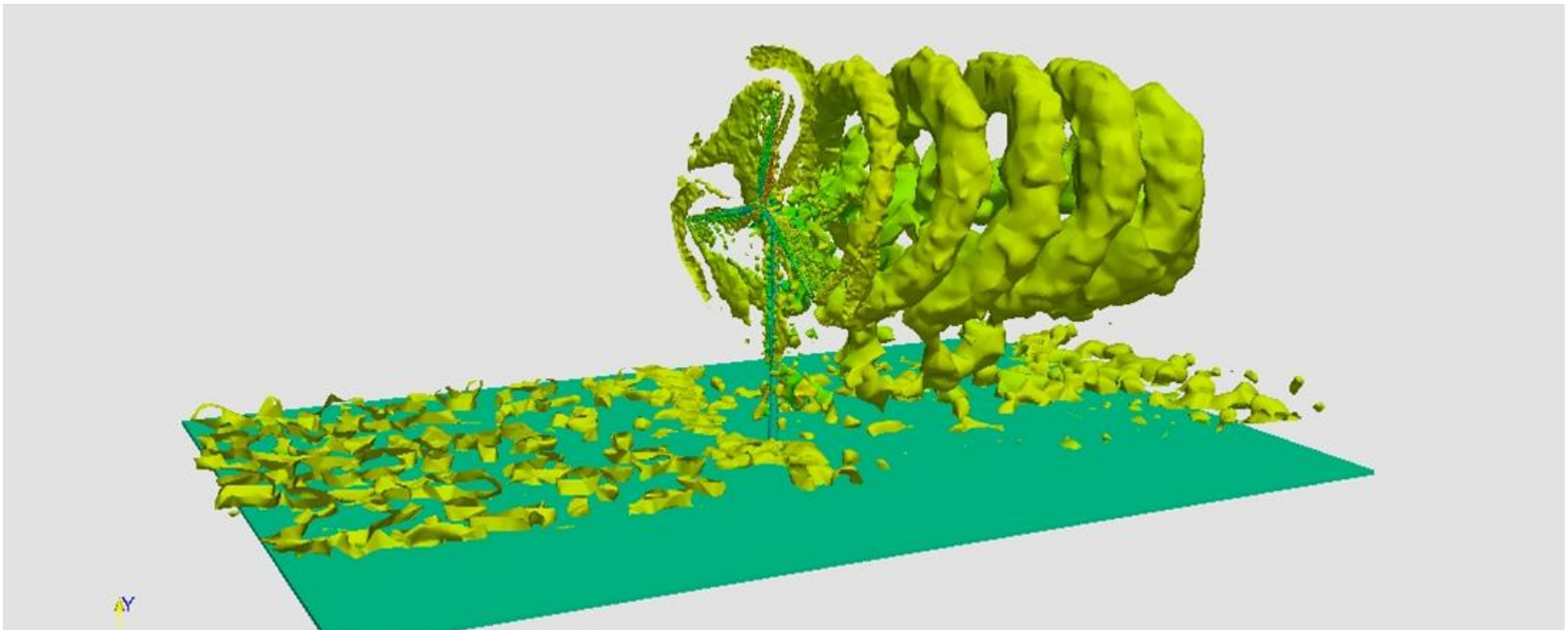
- User defined subroutines for RANS modeling.

### **OpenFoam**

- Wind turbine blade simulation. Rotating imbedded mesh.

## Wind Turbine Calculations with OpenFoam

Spin indicator  
= second invariant of the strain tensor



- Runs on 8-16 CPUs
- No major issues



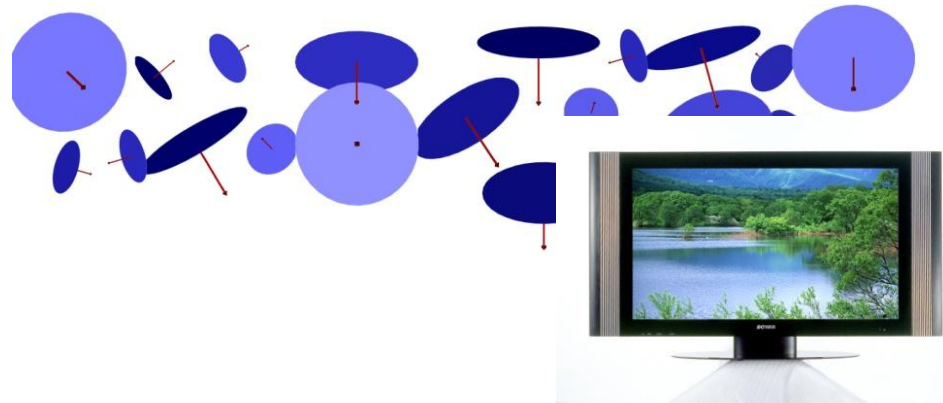
## Eddy Collision Model Overview

### **Assumption:**

**Turbulent Flow = Flow of a Colloidal suspension of disk-like spinning objects.**



**Pouring Spherical objects results in RANS eqns.**

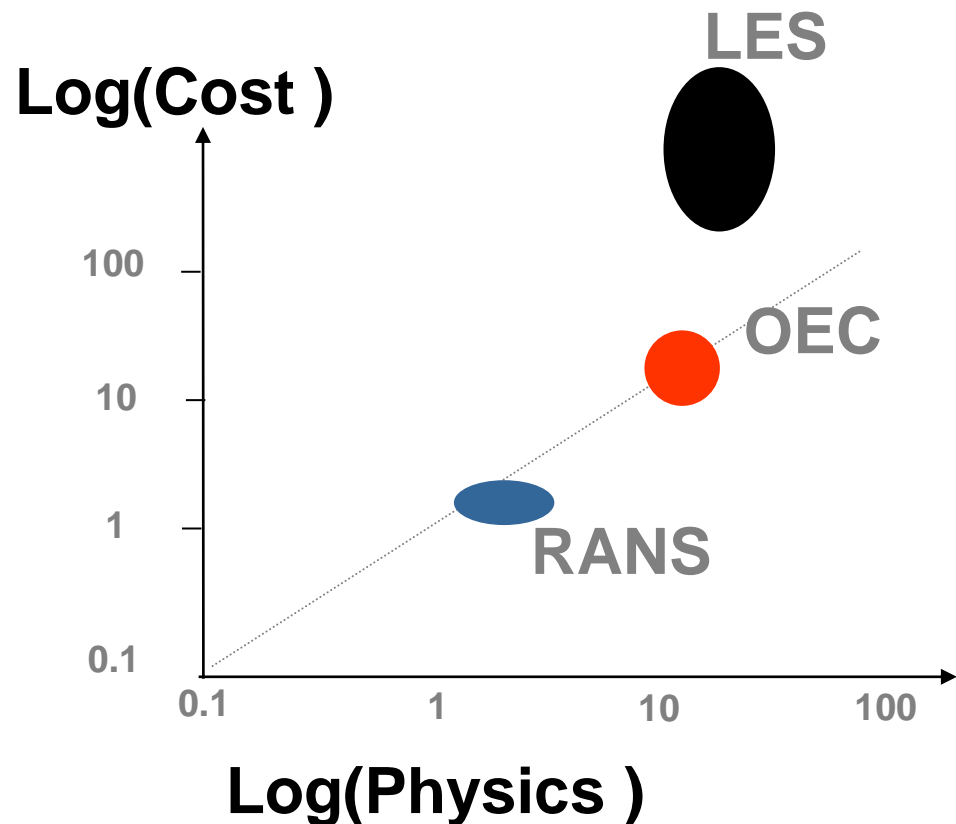


**Pouring a concentrated Disk suspension results in OEC model**



# Review of OEC Model Properties

- Cost roughly about  $10 \times k/e$ .
- Four model constants.
- Realizable, Material Frame Indifferent, Galilean Invariant, Exact in linear limit, etc.



# PDE Formulation

$$\frac{Dq_i}{Dt} = -q_k \bar{u}_{k,i} - \frac{1}{3} \left( \alpha \nu \overline{q^2} + \frac{1}{\tau_R} \right) q_i - (A_i + B_i) + \frac{1}{3} \left[ (\nu + \nu_t) q_{i,k} \right]_{,k} + W_i$$

**Eddy Size and  
Orientation (vector)**

$$\begin{aligned} \frac{DR_{ij}}{Dt} = & \left[ \bar{u}_{i,k} + \left( \frac{q_i q_l}{q^2} - \delta_{il} \right) 2\bar{u}_{l,k}^* \right] R_{kj} + \left[ \bar{u}_{j,k} + \left( \frac{q_j q_l}{q^2} - \delta_{jl} \right) 2\bar{u}_{l,k}^* \right] R_{ki} - \left( \alpha \nu \overline{q^2} + \frac{1}{\tau_R} \right) R_{ij} \\ & - A_{ij} + M_{ij} + \left[ (\nu + \nu_t) R_{ij,k} \right]_{,k} - D(\nu + \nu_t) \left[ \frac{R_{ij}}{K} \right]_{,k} (K)_{,k} - E(\nu + \nu_t) \frac{(K)_{,k}}{K} \frac{(K)_{,k}}{K} R_{ij} + W_{ij} \end{aligned}$$

**Eddy  
Velocity  
Fluctuation  
(tensor)**

- **Global Variables (sum many eddies – 20-50)**

$$\tilde{R}_{ij} = \frac{1}{N} \sum R_{ij}$$

$$\nu_T = \sqrt{\sum \frac{1}{2} R_{ii}^2 / \sum R_{ii} q^2}$$

# Open Foam Formulation

$$\frac{Dq_i}{Dt} = -q_k \bar{u}_{k,i} - \frac{1}{3} \left( \alpha \nu \overline{q^2} + \frac{1}{\tau_R} \right) q_i - (A_i + B_i) + \frac{1}{3} \left[ (\nu + \nu_t) q_{i,k} \right]_{,k} + W_i$$



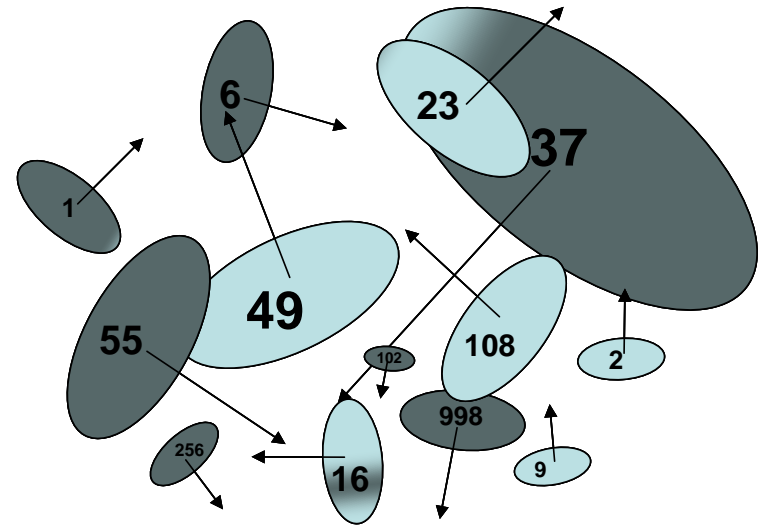
```
fvm::ddt(qiINT)
- (1.0/3.0)*fvm::laplacian(dEff(), qiINT)
+ (1.0/3.0)*fvm::SuSp((alpha*nu()*qsq + tauR), qiINT)
==
- fvc::div(phi_, qiINT)
- ( qiINT & fvc::grad(U) )
- ( Ai + Bi )
```

**Implicit terms on the left-hand side.**

**Explicit terms on the right-hand side.**

## First Challenge: Multiple Eddies

- **The Number of Eddies for each physical location is arbitrary.**
- **10 is minimal necessary.**
- **100 is usually very good.**



**Pointer lists  
are employed  
to keep track  
of eddies**

$\text{Rij\_}[eddy][cell].xx()$  ← Component (11 in this case)  
↑  
Location in mesh  
Pointer list with an entry for every eddy

## Multiple Eddies: OpenFoam Solution

```
forAll(initOrientations_,i) {  
    ...  
    solveqR(i, qi_[i], ...);  
    ...  
}
```

This system allows us to write generalized functions which handle any number of eddy vectors.

```
void OEC::solveqR(int i, volVectorField qiINT, ...) {  
    ...  
    tmp<fvVectorMatrix> qEqn  
    (  
        fvm::ddt(qiINT) = ...  
    );  
    ...  
    solve(qEqn, mesh_.solver("q"));  
    ...  
}
```

The model can be implemented on a per-eddy basis.

Averaging all of the entities in a given pointer list is also easy, which is good because all we really care about is the average R, K, etc.

## Second Challenge: Tensors

- No gradient of a rank 2 (and higher) tensor

$$-D(v + v_t) \left[ \frac{R_{ij}}{K} \right]_{,k} (K)_{,k} \longrightarrow \text{fvc::grad(R)}$$

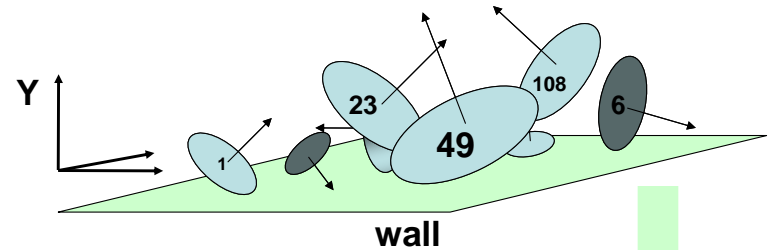
### Solution:

Break it  
into vectors

```
forAll (mesh_.C(), cell)          // internal cells
{
    Rx[cell].x() = Rtmp[cell].xx();
    Rx[cell].y() = Rtmp[cell].xy();
    Rx[cell].z() = Rtmp[cell].xz();
    ...
    gradKgradR[cell].xx() = ( gradK[cell].x()*gradRx[cell].xx()
                             + gradK[cell].y()*gradRx[cell].xy()
                             + gradK[cell].z()*gradRx[cell].xz() );
    gradKgradR[cell].yy() = ( gradK[cell].x()*gradRy[cell].yx()
                             + gradK[cell].y()*gradRy[cell].yy()
                             + gradK[cell].z()*gradRy[cell].yz() );
    gradKgradR[cell].zz() = ( gradK[cell].x()*gradRz[cell].zx()
                             + gradK[cell].y()*gradRz[cell].zy()
                             + gradK[cell].z()*gradRz[cell].zz() );
}
```

## Third Challenge: Boundary Conditions

- On wall, the boundary conditions are mixed.



This is for an xz-wall.  
We currently can not do walls that are not aligned with the tensor coordinate directions.

$$R_{ij}|_{\text{slip-wall}} \rightarrow \begin{bmatrix} \frac{\partial R_{11}}{\partial y} = 0 & R_{12} = 0 & \frac{\partial R_{13}}{\partial y} \\ & R_{22} = 0 & R_{23} = 0 \\ & & \frac{\partial R_{33}}{\partial y} \end{bmatrix}$$

$$q_i|_{\text{wall}} \rightarrow \begin{bmatrix} q_1 = 0 \\ \frac{\partial q_2}{\partial y} = 0 \\ q_3 = 0 \end{bmatrix}$$



## Last Challenge: Stable Time Marching

- Many source terms have no `fvm::` (implicit) implementation.
- Some explicit source terms can be unstable with Explicit Euler time advancement.

### Solution:

- Write a RK3 solver.
- Modify equations with explicit time derivative
- Use FOAM's `.storeOldTime()` to save the old time values.

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(
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    + (1.0/3.0)*fvm::SuSp((alpha*nu()*qsq + tauR), qiINT)
    ==
    - fvc::div(phi_, qiINT)
    - ( qiINT & GU_ )
    - ( Ai + Bi )
    + ( (qiTMPINT - qiINT) / mesh_.time().deltaT() ) // RK3 correction term
);

//...

solve(qEqn, mesh_.solver("q"));
```

## Last Challenge: Stable Time Marching

- Many source terms have no fvm:: (implicit)

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);

//...

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```

- Use FOAM's `.storeOldTime()` to save the old time values.

## Last Observation:

- Gradient of a vector

$$a_{i,j} = \begin{bmatrix} \frac{\partial a_1}{\partial x_1} & \frac{\partial a_2}{\partial x_1} \\ \frac{\partial a_1}{\partial x_2} & \frac{\partial a_2}{\partial x_2} \end{bmatrix} = \begin{bmatrix} a_{1,1} & a_{2,1} \\ a_{1,2} & a_{2,2} \end{bmatrix} = \begin{bmatrix} g_{11} & g_{12} \\ g_{21} & g_{22} \end{bmatrix} = \partial_i a_j$$

## Summary:

- OEC is implemented in OpenFoam.

