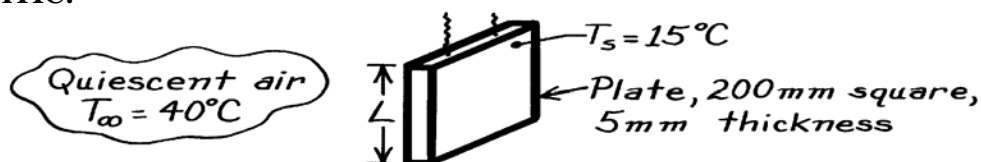


## PROBLEM 9.8

**KNOWN:** Square aluminum plate at 15°C suspended in quiescent air at 40°C.

**FIND:** Average heat transfer coefficient by two methods – using results of boundary layer similarity and results from an empirical correlation.

**SCHEMATIC:**



**ASSUMPTIONS:** (1) Uniform plate surface temperature, (2) Quiescent room air, (3) Surface radiation exchange with surroundings negligible, (4) Perfect gas behavior for air,  $\beta = 1/T_f$ .

**PROPERTIES:** Table A-4, Air ( $T_f = (T_s + T_\infty)/2 = (40 + 15)^\circ\text{C}/2 = 300\text{K}$ , 1 atm):  $\nu = 15.89 \times 10^{-6} \text{ m}^2/\text{s}$ ,  $k = 0.0263 \text{ W/m}\cdot\text{K}$ ,  $\alpha = 22.5 \times 10^{-6} \text{ m}^2/\text{s}$ ,  $\text{Pr} = 0.707$ .

**ANALYSIS:** Calculate the Rayleigh number to determine the boundary layer flow conditions,

$$\text{Ra}_L = g \beta \Delta T L^3 / \nu \alpha$$

$$\text{Ra}_L = 9.8 \text{ m/s}^2 (1/300\text{K}) (40 - 15)^\circ\text{C} (0.2\text{m})^3 / (15.89 \times 10^{-6} \text{ m}^2/\text{s}) (22.5 \times 10^{-6} \text{ m}^2/\text{s}) = 1.827 \times 10^7$$

where  $\beta = 1/T_f$  and  $\Delta T = T_\infty - T_s$ . Since  $\text{Ra}_L < 10^9$ , the flow is laminar and the *similarity solution* of Section 9.4 is applicable. From Eqs. 9.21 and 9.20,

$$\overline{\text{Nu}}_L = \frac{\bar{h}_L L}{k} = \frac{4}{3} (\text{Gr}_L / 4)^{1/4} g(\text{Pr})$$

$$g(\text{Pr}) = \frac{0.75 \text{Pr}^{1/2}}{\left[ 0.609 + 1.221 \text{Pr}^{1/2} + 1.238 \text{Pr} \right]^{1/4}}$$

and substituting numerical values with  $\text{Gr}_L = \text{Ra}_L / \text{Pr}$ , find

$$g(\text{Pr}) = 0.75 (0.707)^{1/2} / \left[ 0.609 + 1.22 (0.707)^{1/2} + 1.238 \times 0.707 \right]^{1/4} = 0.501$$

$$\bar{h}_L = \left( \frac{0.0263 \text{ W/m}\cdot\text{K}}{0.20\text{m}} \right) \times \frac{4}{3} \left( \frac{1.827 \times 10^7 / 0.707}{4} \right)^{1/4} \times 0.501 = 4.42 \text{ W/m}^2 \cdot \text{K} <$$

The appropriate empirical correlation for estimating  $\bar{h}_L$  is given by Eq. 9.27,

$$\overline{\text{Nu}}_L = \frac{\bar{h}_L L}{k} = 0.68 + \frac{0.670 \text{Ra}_L^{1/4}}{\left[ 1 + (0.492 / \text{Pr})^{9/16} \right]^{4/9}}$$

$$\bar{h}_L = (0.0263 \text{ W/m}\cdot\text{K} / 0.20\text{m}) \left[ 0.68 + 0.670 (1.827 \times 10^7)^{1/4} / \left[ 1 + (0.492 / 0.707)^{9/16} \right]^{4/9} \right]$$

$$\bar{h}_L = 4.51 \text{ W/m}^2 \cdot \text{K} <$$

**COMMENTS:** The agreement of  $\bar{h}_L$  calculated by these two methods is excellent. Using the Churchill-Chu correlation, Eq. 9.26, find  $\bar{h}_L = 4.87 \text{ W/m}\cdot\text{K}$ . This relation is not the most accurate for the laminar regime, but is suitable for both laminar and turbulent regions.