

CEE 577: Surface Water Quality Modeling

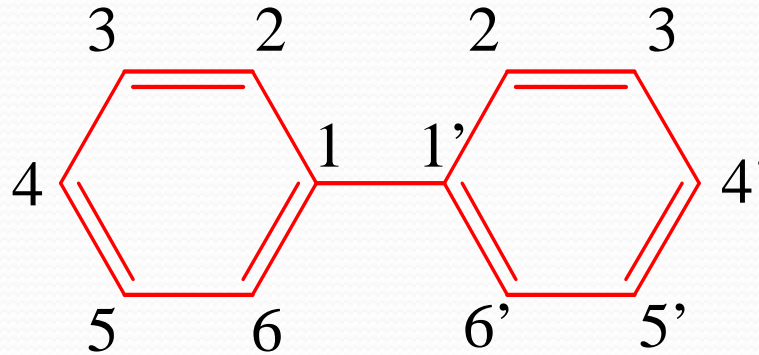
Lecture #36

Toxics: PCBs in the Great Lakes
(Jeremiason et al., 1994)

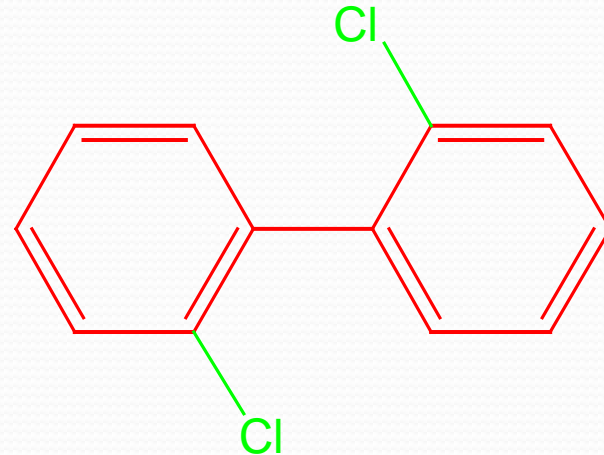
Homologs (11)
Isomers (1-46)
Congeners (209)

What are the PCBs

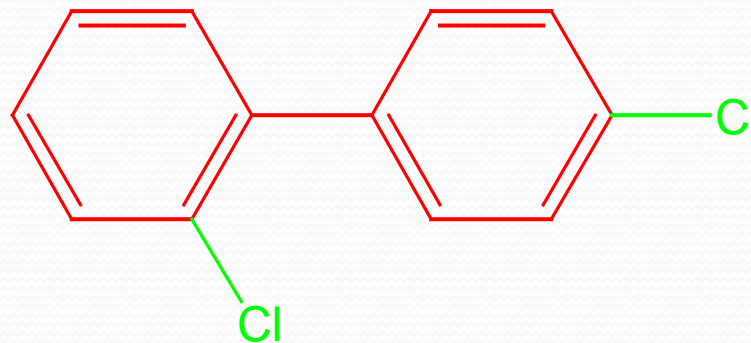
- Biphenyl



- 2,2' - Dichlorobiphenyl



- 2,3' - Dichlorobiphenyl



History

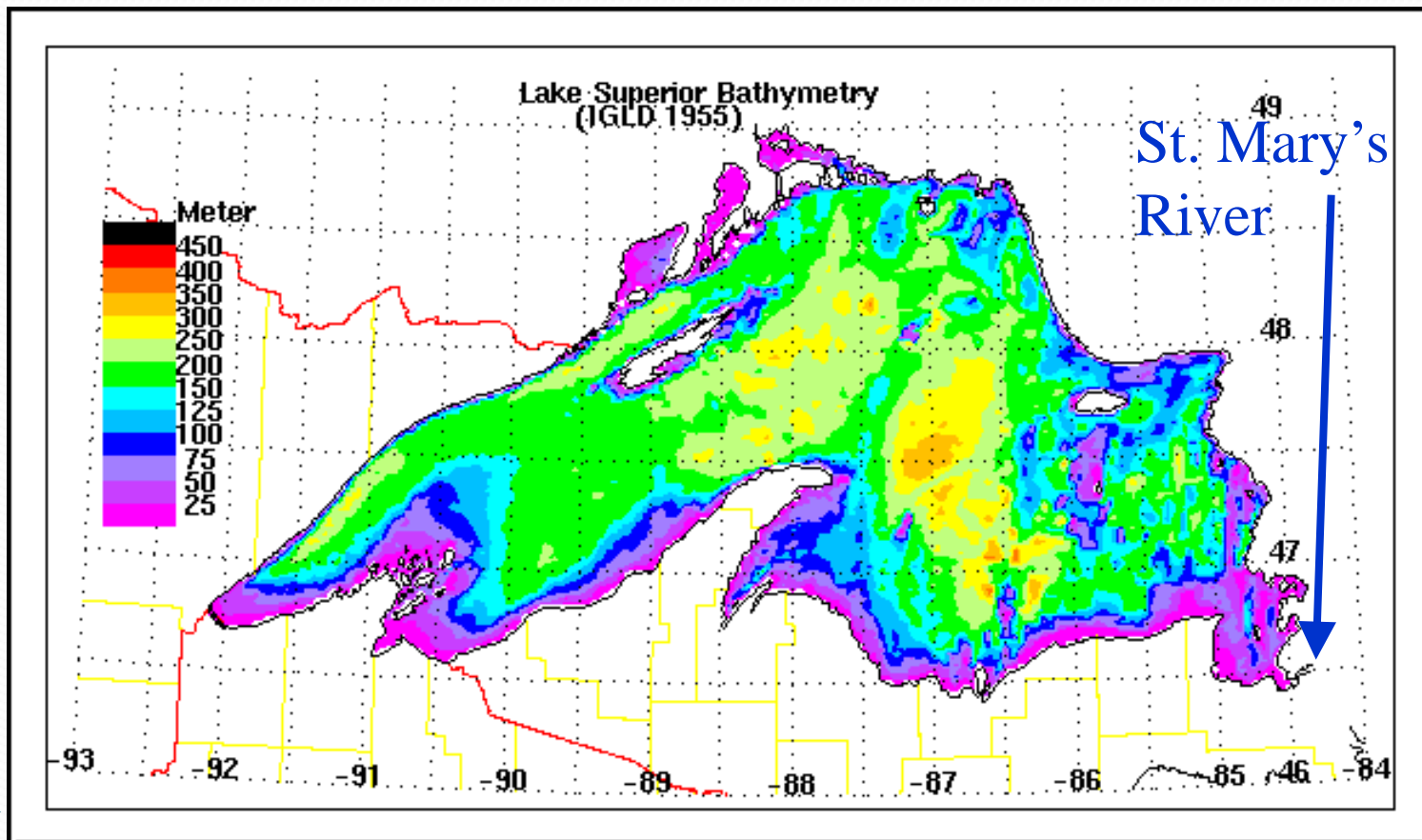
- 1930: Monsanto is major US producer
- 1970: Monsanto decides to sell PCBs only for closed use
- 1975: NY State warns public about salmon and bass in Hudson
- 1979: PCB manufacture banned in US
- 1982: NY State begins dredging “hot spots”
- 1990: all PCB-containing equipment must be removed from US public buildings

Arochlor Mixtures

- Arochlor 12xx (xx=% chlorine)
 - 1221: 50% Cl₁, 35% Cl₂
 - 1232: 26% Cl₁, 29% Cl₂, 24% Cl₃
 - 1242: 13% Cl₂, 45% Cl₃, 31% Cl₄
 - 1248: 49% Cl₄, 27% Cl₅
 - 1254: 15% Cl₄, 53% Cl₅, 26% Cl₆
 - 1260: 12% Cl₅, 42% Cl₆, 38% Cl₇
 - 1262: no data
 - 1268: no data

PCBs in the Lake Superior

- Reference: “PCBs in Lake Superior, 1978-1992: Decrease in Water Concentrations Reflect Loss by Volatilization,” by Jeremiason, Hornbuckle and Eisenreich, [Environmental Science and Technology](#), 28:903 (1994)



Empirical Models

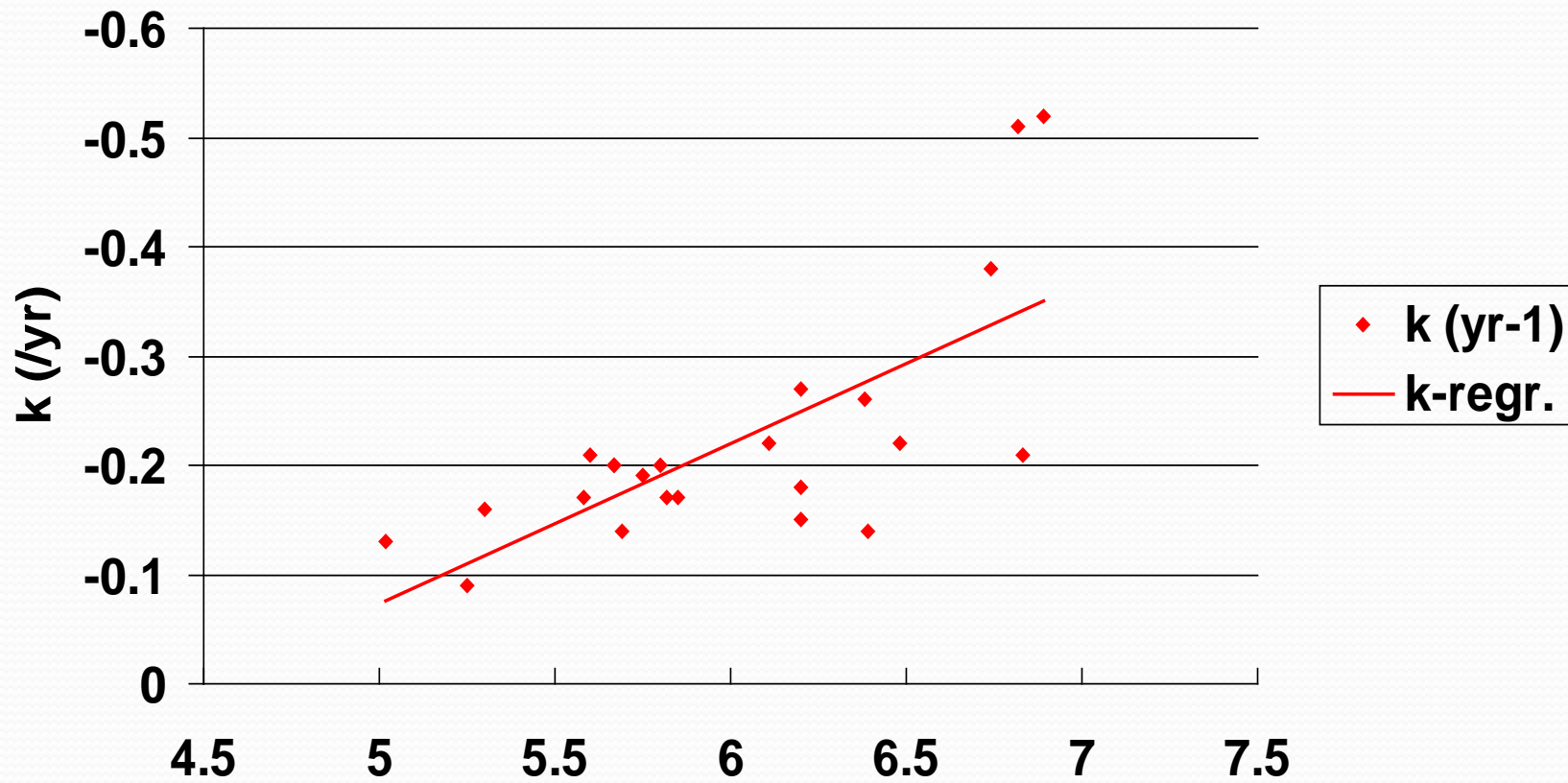
$$\sum_{25} PCB = \left(\sum_{25} PCB_o \right) e^{-0.20t}$$

$$\sum_{82} PCB = \left(\sum_{82} PCB_o \right) e^{-0.22t}$$

- Data tell us that about 26,500 kg has been lost from the water column between 1980 and 1992

Loss rate and K_{ow} 's

Log Kow



Areal Sediment Burden (mass)

- Estimated at 4900 kg in 1986
 - using data from sediment cores
 - relatively small compared to total lost from water column (26,500 kg from '80 to '92)

$$\sum PCB_{areal} = \sum PCB_i (1 - \phi_i) \rho_s z_i$$

PCB conc. (ng/g-dry sediment) in depth increment "i"

Thickness of depth increment "i"

Porosity of increment "i"

Inputs

- Riverine
 - Known Q
 - Estimate c from analysis of pristine rain
- Other
 - estimates from industrial, municipal, (urban) runoff and storm sewer flows gives a combined total of about 40 kg/yr

$$\begin{aligned}W &= Qc \\ &= 5.4 \times 10^{13} \text{ L / yr} (2 \text{ ng / L}) \\ &= 110 \text{ kg / yr}\end{aligned}$$

Inputs (cont.)

- Direct Atmospheric deposition

- wet deposition

precipitation Surface Area

$$\begin{aligned}
 F_{wet} &= \sum PCB_{T,rain} P(SA) \\
 &= 2ng / L(76cm)8.21 \times 10^{10} m^2 \\
 &= 125kg / yr
 \end{aligned}$$

- dry deposition

- calculated for 4 seasons, then averaged

Dry particle deposition velocity (0.2 cm/s)

$$\begin{aligned}
 F_{dry} &= \sum PCB_{T,air} V_d \phi(SA) f_d \\
 &= 32kg / yr
 \end{aligned}$$

Fraction of year when it is not precipitating (0.9)

Fraction of PCBs associated with particles

Outputs

- Outflow
 - St. Mary's River

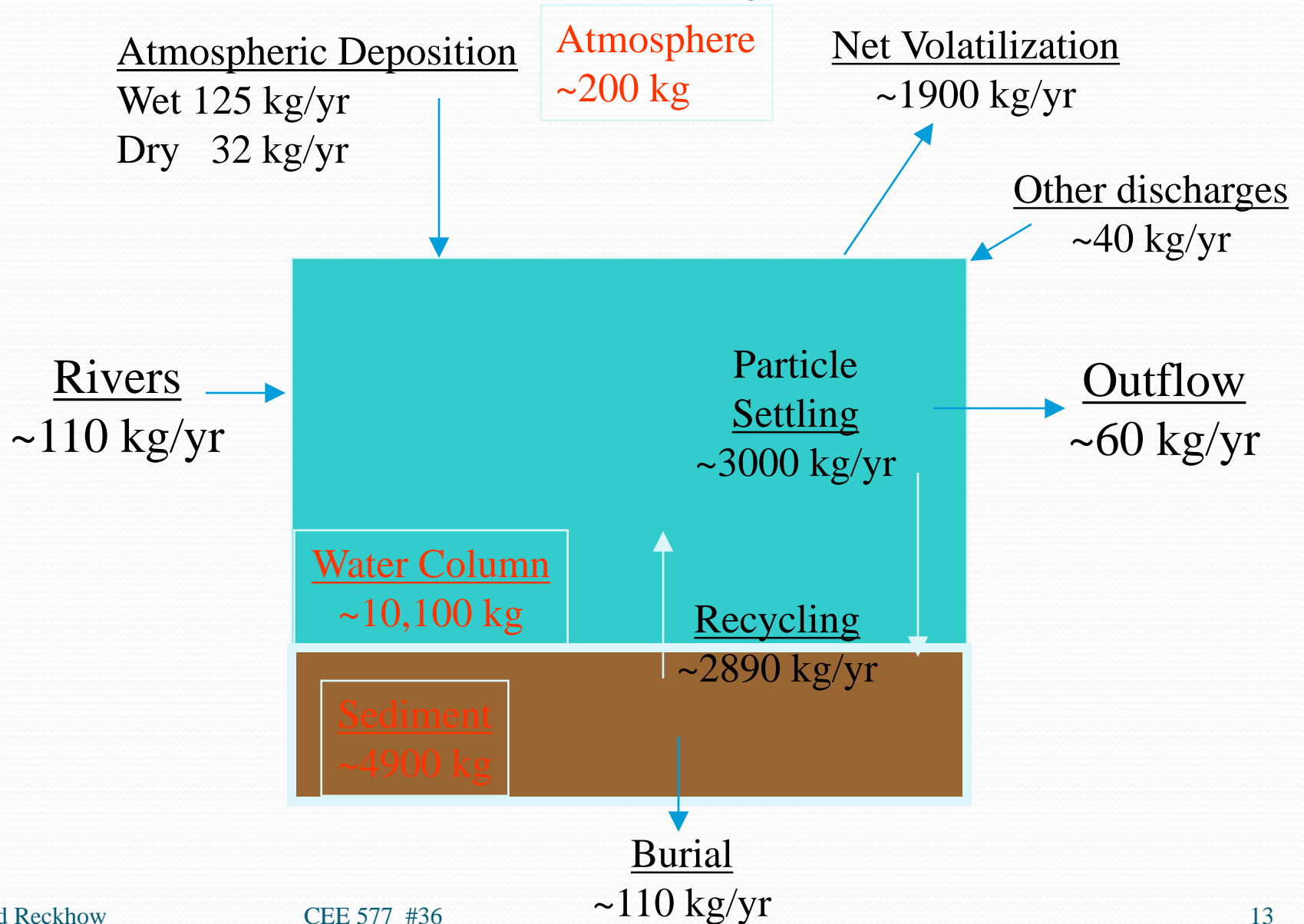
$$W_{outflow} = 7.1 \times 10^{13} \text{ L / yr} (0.84 \text{ ng / L}) = 60 \text{ kg / yr}$$

- Burial (net loss to sedimentation)
 - estimated at 110 kg/yr from sediment cores collected in 1986 and 1990
- Net Volatilization
 - true volatilization minus gas absorption
 - assumed to account for missing flux

Reactions

- NONE!
 - “evidence does not exist to support PCB degradation in Lake Superior or any other oligotrophic, aerobic system exhibiting low ambient concentrations”

PCB Mass Balance in Lake Superior, 1986



Congener-specific sedimentation

- Calculation of first-order net sedimentation rate

Mass sedimentation rate (mg/cm²/yr)

$$k_{sed} = \frac{\left[\frac{W_{sed}}{INV_w} \right] f_p}{RR}$$

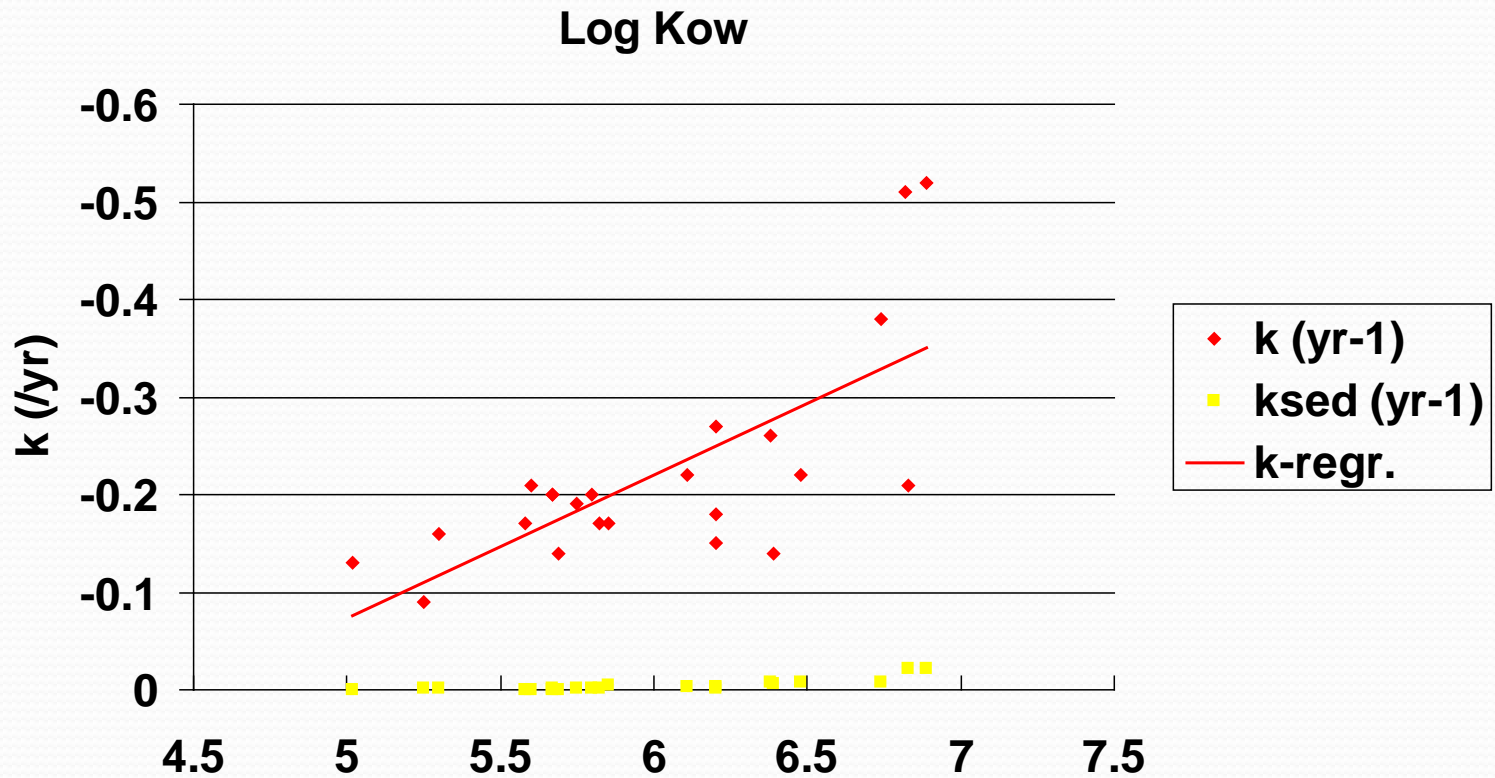
Inventory (or areal TSS)

Fraction particulate

The diagram shows the equation $k_{sed} = \frac{\left[\frac{W_{sed}}{INV_w} \right] f_p}{RR}$ with a light blue background. Red arrows point from text labels to the variables in the equation: 'Inventory (or areal TSS)' points to INV_w , 'Fraction particulate' points to f_p , and 'Recycling ratio = downward flux (from sed trap) divided by the accumulation in the sediment' points to RR . The text 'Mass sedimentation rate (mg/cm²/yr)' is positioned above the equation.

Recycling ratio = downward flux (from sed trap)
divided by the accumulation in the sediment

Sedimentation vs overall loss rate



Two Film Volatilization Model

- Jeremiason's equation $k_{vol} = \frac{K_{ol}}{h} f_w$

- Same as Chapra's $k_v = \frac{v_v}{H_1} f_{d1}$

- Where:

$$\frac{1}{K_{ol}} = \frac{RT}{k_a H} + \frac{1}{k_w}$$

Estimating 2-film parameters

- The gas film coefficient

$$k_{a,H_2O} = 0.2u_{10} + 0.3$$

$$k_{a,PCB} = k_{a,H_2O} \left(\frac{D_{PCB,air}}{D_{H_2O,air}} \right)^{0.61}$$

- The liquid film coefficient

$$k_{w,CO_2} = 0.45u_{10}^{1.64}$$

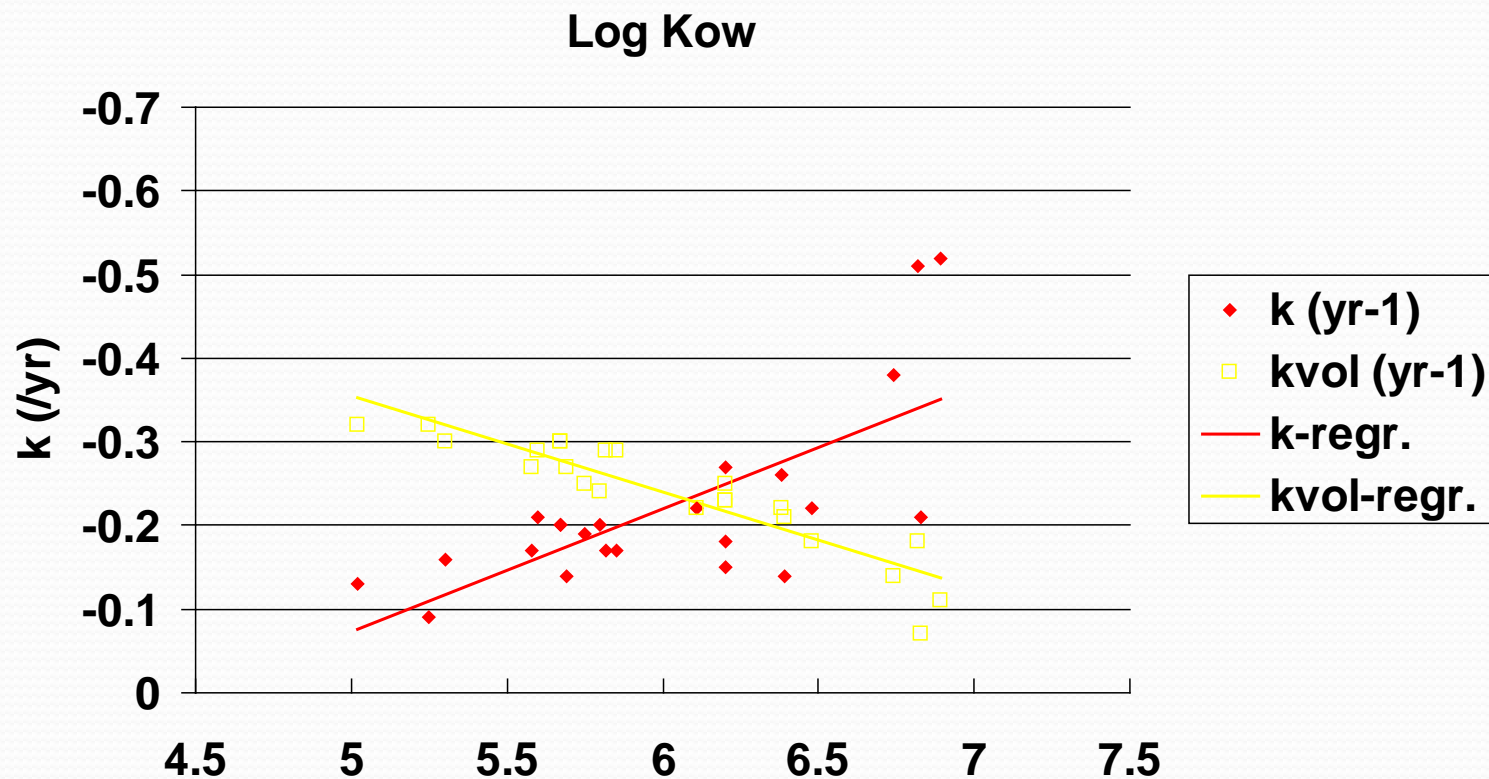
$$k_{w,PCB} = k_{w,CO_2} \left(\frac{Sc_{PCB}}{Sc_{CO_2}} \right)^{-0.5}$$

Kinetic viscosity: molecular diffusivity

$$Sc = \frac{\mu}{\rho \cdot D_v}$$

Schmidt Number

Volatilization vs overall loss rate



- To next lecture