

CEE 577: Surface Water Quality Modeling

Lecture #18

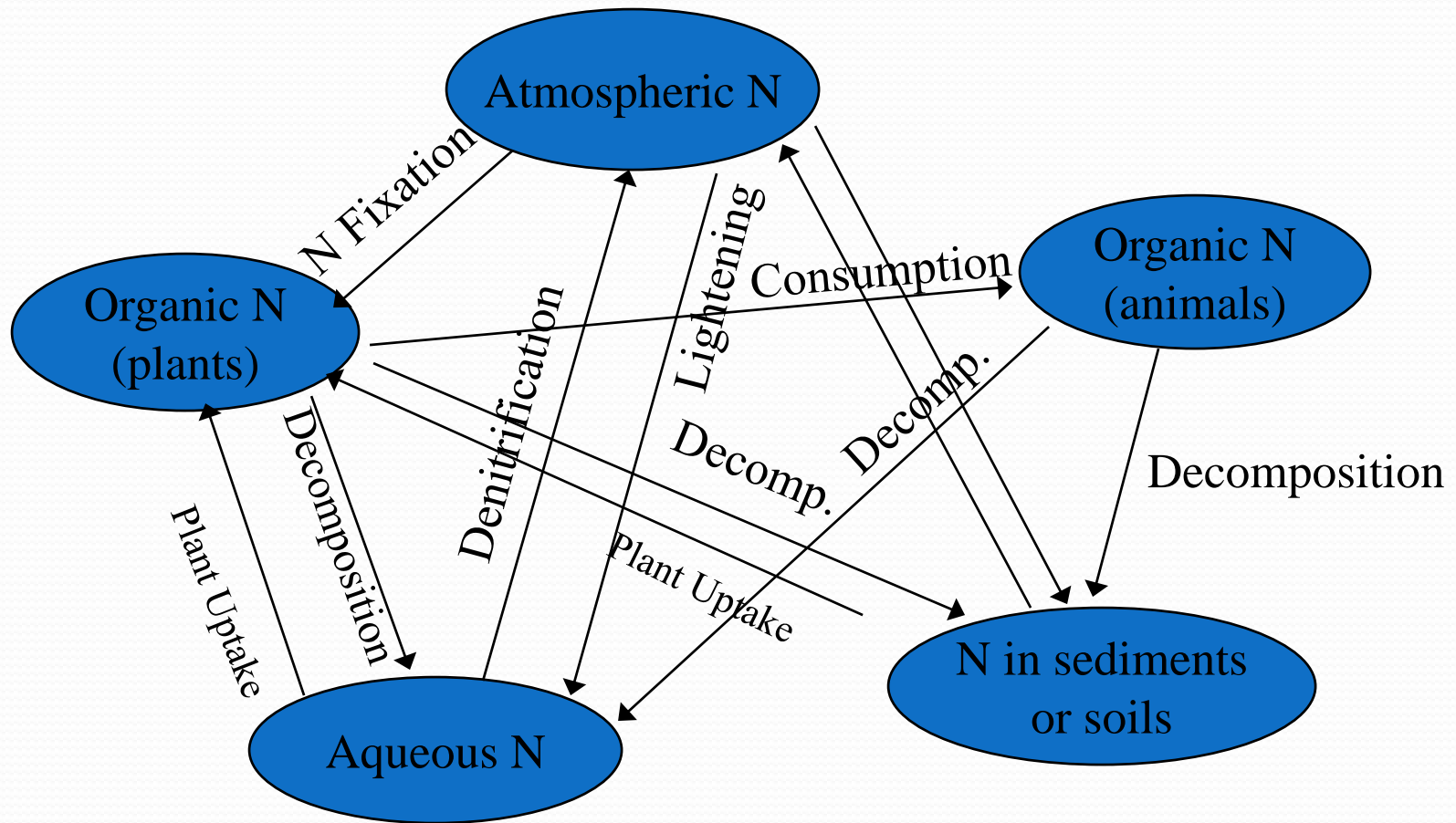
Streeter-Phelps: Distributed Sources &
Nitrogen

(Chapra, L22 & L23)

Nitrogen (Chapra L23)

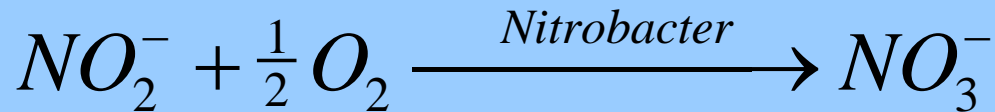
- Nitrification/Denitrification
 - nitrification: oxygen consuming
 - denitrification: anaerobic, form N_2
- Eutrophication
 - stimulates plant growth
- Nitrate pollution
 - from fertilizers and nitrification
- Ammonia toxicity (NH_3 form)

Nitrogen Cycle



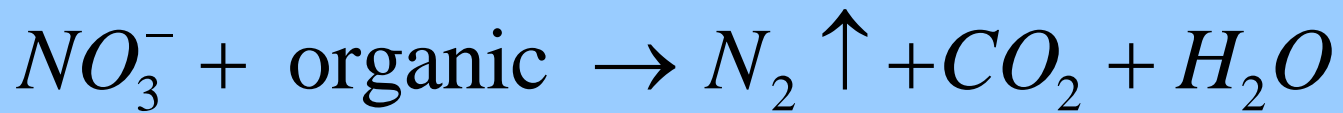
Nitrification/Denitrification

Nitrification: will satisfy NBOD and NH_3 toxicity



Can be combined with traditional activated sludge so that NBOD is removed along with CBOD; occurs naturally in surface waters

Denitrification: will remove nitrate, nutrient control



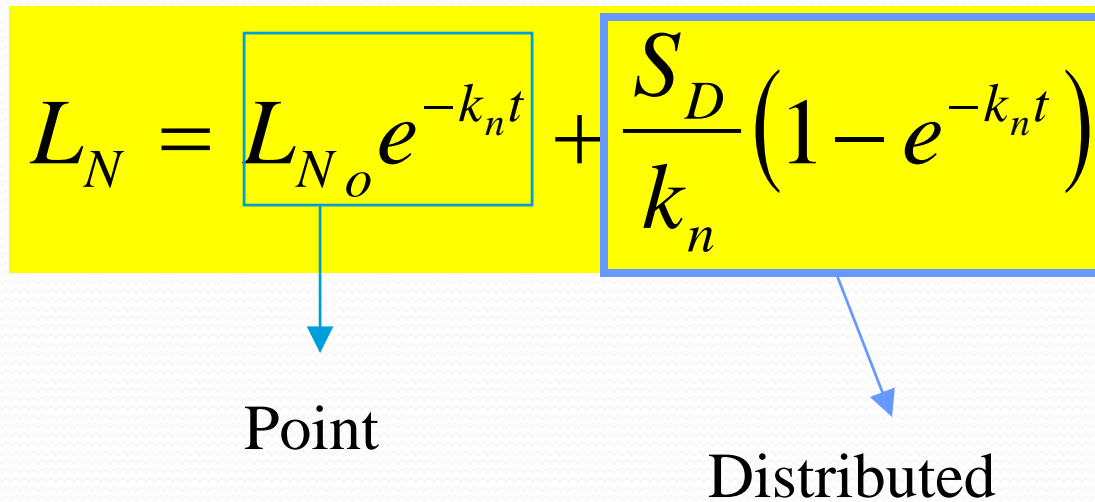
Requires an **anaerobic** environment

Modeling Nitrification

$$L_N = L_{N_o} e^{-k_n t} + \frac{S_D}{k_n} (1 - e^{-k_n t})$$

Point

Distributed

The equation is presented on a yellow background. The first term, $L_{N_o} e^{-k_n t}$, is enclosed in a blue box, and a blue arrow points from this box down to the word "Point". The second term, $\frac{S_D}{k_n} (1 - e^{-k_n t})$, is enclosed in a blue box, and a blue arrow points from this box down to the word "Distributed".

$$L_N = 4.57 * \text{TKN}$$

In-class problem I

- A poorly treated municipal wastewater is discharged into Evergreen Brook at milepoint zero. In addition there is a continuous discharge of soluble BOD from a series of hog farms extending from milepoint zero to mile 25.
 - The WWTP discharges sufficient BOD such that there is 12 mg/L BOD at the point of mixing, 30% of which is particulate
 - The hog farms release 5 g-BOD/d for every foot of stream length
 - The stream can be considered to have a uniform depth of 4 ft, a width of 22 ft and a rocky bottom. Velocity is 3 mi/d.
 - Assume a BOD settling rate of 1.2 d^{-1}
- What is the BOD concentration 10 miles downstream and how much originates from each source (WWTP vs hog farm)?

In-class problem II

- First determine distributed loading term

$$S_d = \frac{S_d''}{A_c} = \frac{S_d'}{H} = \frac{5 \text{ g/ft-d}}{4 \text{ ft}(22 \text{ ft})} \left(\frac{1 \text{ ft}^3}{28.3 \text{ L}} \right) = 2.0 \frac{\text{mg}}{\text{L-d}}$$

- Next estimate deoxygenation rate

$$k_d = C \left(\frac{H}{8} \right)^{-0.434} = 0.3 \left(\frac{4}{8} \right)^{-0.434} = 0.405 \text{ d}^{-1}$$

- Then formulate BOD model

$$L = L_o e^{-k_r t} + \frac{S_D}{k_r} (1 - e^{-k_r t})$$

deoxygenation only, no settling

$$= 12(0.3)e^{-1.605x/U} + 12(0.7)e^{-0.405x/U} + \frac{2}{0.405} (1 - e^{-0.405x/U})$$

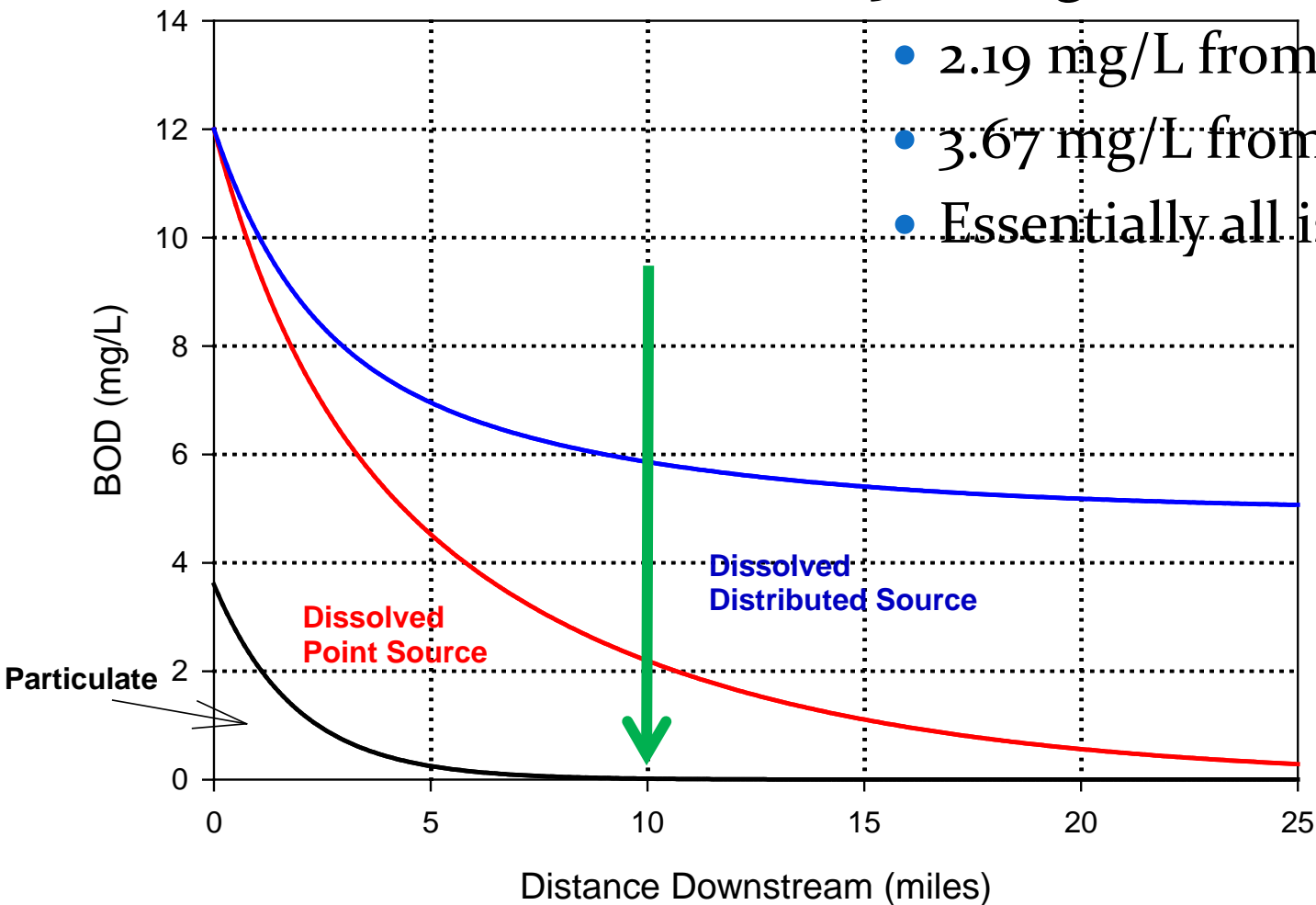
In-class problem II

• 5.86 mg/L @10 mi

• 2.19 mg/L from WWTP

• 3.67 mg/L from hog farms

• Essentially all is dissolved



Full Equation

$$D = D_o e^{-k_a t} + \frac{k_d L_o}{k_a - k_r} (e^{-k_r t} - e^{-k_a t})$$

$$+ \frac{k_n L_{No}}{k_a - k_n} (e^{-k_n t} - e^{-k_a t})$$

Point NBOD

$$+ \frac{-P + R + \left(\frac{S'_B}{H} \right)}{k_a} (1 - e^{-k_a t})$$

$$+ \frac{k_d S_d}{k_r k_a} (1 - e^{-k_a t}) - \frac{k_d S_d}{k_r (k_a - k_r)} (e^{-k_r t} - e^{-k_a t})$$

$$+ \frac{k_n S_{Nd}}{k_n k_a} (1 - e^{-k_a t}) - \frac{k_n S_{Nd}}{k_n (k_a - k_n)} (e^{-k_n t} - e^{-k_a t})$$

Distributed NBOD

Sample Problem (T&M, pg.309)

- Problem

- Determine the maximum allowable ultimate oxygen demand (UOD) in the effluent entering the stream if the DO concentration is to equal or exceed 5 mg/L. Assume the effluent DO is equal to the stream's DO saturation concentration.

$$Q_u = 20 \text{ cfs}$$

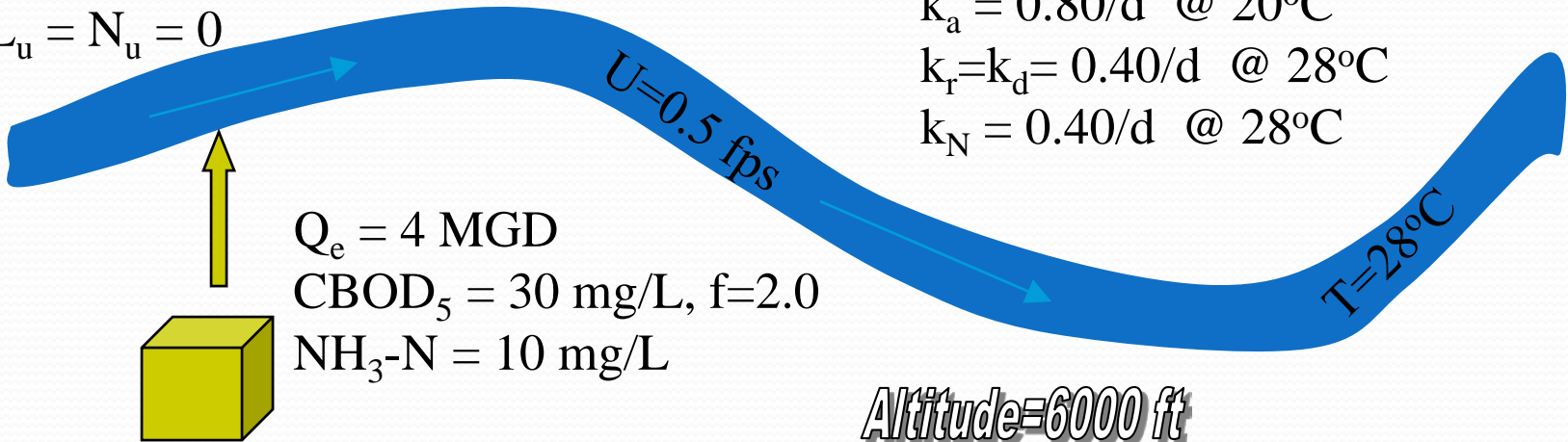
$$c_u = c_s$$

$$L_u = N_u = 0$$

$$k_a = 0.80/\text{d} \text{ @ } 20^\circ\text{C}$$

$$k_r = k_d = 0.40/\text{d} \text{ @ } 28^\circ\text{C}$$

$$k_N = 0.40/\text{d} \text{ @ } 28^\circ\text{C}$$



Problem (cont.)

- Analysis of existing conditions
 - Loading
 - BOD and NBOD may be treated as one UOD load since the decay rates are the same in the stream. Assume only the ammonia is significant in the NBOD.

$$\begin{aligned} UOD(mg / L) &= fxCBOD_5 + 4.57x(NH_3 - N) \\ &= 2.0x30 + 4.57x10 = 105.7mg / L \end{aligned}$$

$$W(UOD) = 4MGDx105.7 \frac{mg}{L} x8.34 = 3530lb / d$$

$$\begin{aligned} L_o &= \frac{W(UOD)}{Q_u + Q_e} = \frac{3530lb / d}{(20cfs + 4(1.548)cfs)5.4} \\ &= 25.0 \frac{mg}{L} \end{aligned}$$

Problem (cont.)

- Adjust Reaction rates to ambient temp.

$$\begin{aligned}k_a &= k_a(20^\circ C) \times \theta^{T-20} \\ &= 0.8(1.024)^{(28-20)} = 0.97 d^{-1} @ 28^\circ C\end{aligned}$$

- Determine t_{crit}

$$\begin{aligned}t_{crit} &= \frac{l}{k_a - k_r} \ln \left[\frac{k_a}{k_r} \left(1 - \frac{D_o(k_a - k_r)}{k_d L_o} \right) \right] \\ &= \frac{l}{0.97 - 0.40} \ln \left[\frac{0.97}{0.40} \left(1 - \frac{0(0.97 - 0.40)}{0.40(25.0)} \right) \right] \\ &= 1.55d\end{aligned}$$

Problem (cont.)

- Then get x_{crit}
- And c_s is:
 - accounting for temp. & altitude
- Finally the c_{min} is:

$$x = Ut = 0.5 \text{ fps} \left(\frac{16.4 \text{ mpd}}{\text{fps}} \right) 1.55d = 12.7 \text{ mi}$$

$$c_s = 6.19 \frac{\text{mg}}{L}$$

$$\begin{aligned} c_{\text{min}} &= c_s - L_o \frac{k_d}{k_a} e^{-k_r t_{\text{crit}}} \\ &= 6.19 - 25.0 \frac{0.40}{0.97} e^{-0.40(1.55)} \\ &= 0.64 \frac{\text{mg}}{L} \end{aligned}$$

Problem (end)

- Determine allowable load, if WQC require 5.0 mg/L minimum D.O.
 - Recognize that the loading:deficit relationship is linear

$$D_{crit} \equiv c_s - c_{min} = L_o \frac{k_d}{k_a} e^{-k_r t_{crit}}$$

Also, t_{crit} is independent of L when $D_o=0$

- so determine allowable L

$$\begin{aligned} \frac{D_{crit}}{L_o} &= \frac{D_{crit(allowable)}}{L_{o(allowable)}} \\ L_{o(allowable)} &= \frac{D_{crit(allowable)} L_o}{D_{crit}} = \frac{1.19(105.7)}{5.55} \\ &= 23 \frac{mg}{L} \end{aligned}$$

Additional notes on WLA

Not from Chapra

- Selecting a model
 - number of dimensions
 - usually 1, major gradients are longitudinal, very minor gradients in lateral and vertical directions
 - sometimes 2, deep rivers or river-run impoundments; use should be justified
 - never 3, except research and a few extraordinary cases

Additional notes on WLA (cont.)

- Loads, sources & sinks
 - Categorize
 - category I - major sources controlling water quality
 - thorough data collection - temporal variation
 - category II - background sources
 - small to moderate data collection
 - necessary data
 - long-term BOD, with nitrification inhibition
 - analysis of all forms of nitrogen
 - org-N, NH₃, NO₂, NO₃

Additional notes on WLA (cont.)

- Time scale
 - steady state
 - quasi-steady state
 - const. loads, constant Q , diurnal DO variations due to photosynthesis
 - const. loads, variable Q
 - variable loads, constant Q
 - others
 - Fully time-variable analysis

Additional notes on WLA (cont.)

- Design Conditions
 - 7Q₁₀ - summer
 - generally endorsed by USEPA
 - Spring Floods - large event
 - storm intensity, sequences, recessional hydrograph
 - Ice cover - winter
- Spatial Extent
 - well into the zone of recovery

Additional notes on WLA (cont.)

- Dispersion (is it significant?)

- calculate E

- from slope

mi²/d

- from dye studies

- calculate dimensionless estuary #

- use Chapra's criteria

- n < 0.1, advection predominates
 - n > 10, diffusion predominates

- or calculate reaeration/deoxygenation ratio & use O'Connor figure

$$\phi = \frac{k_a}{k_d}$$

$$E = 3.4 \times 10^{-5} \frac{UB^2}{HU^*}$$

ft/s (pointing to U), ft (pointing to B), ft (pointing to H), ft (pointing to U*)

$$U^* = \sqrt{gHS}$$

$$n = \frac{k_d E}{U^2}$$

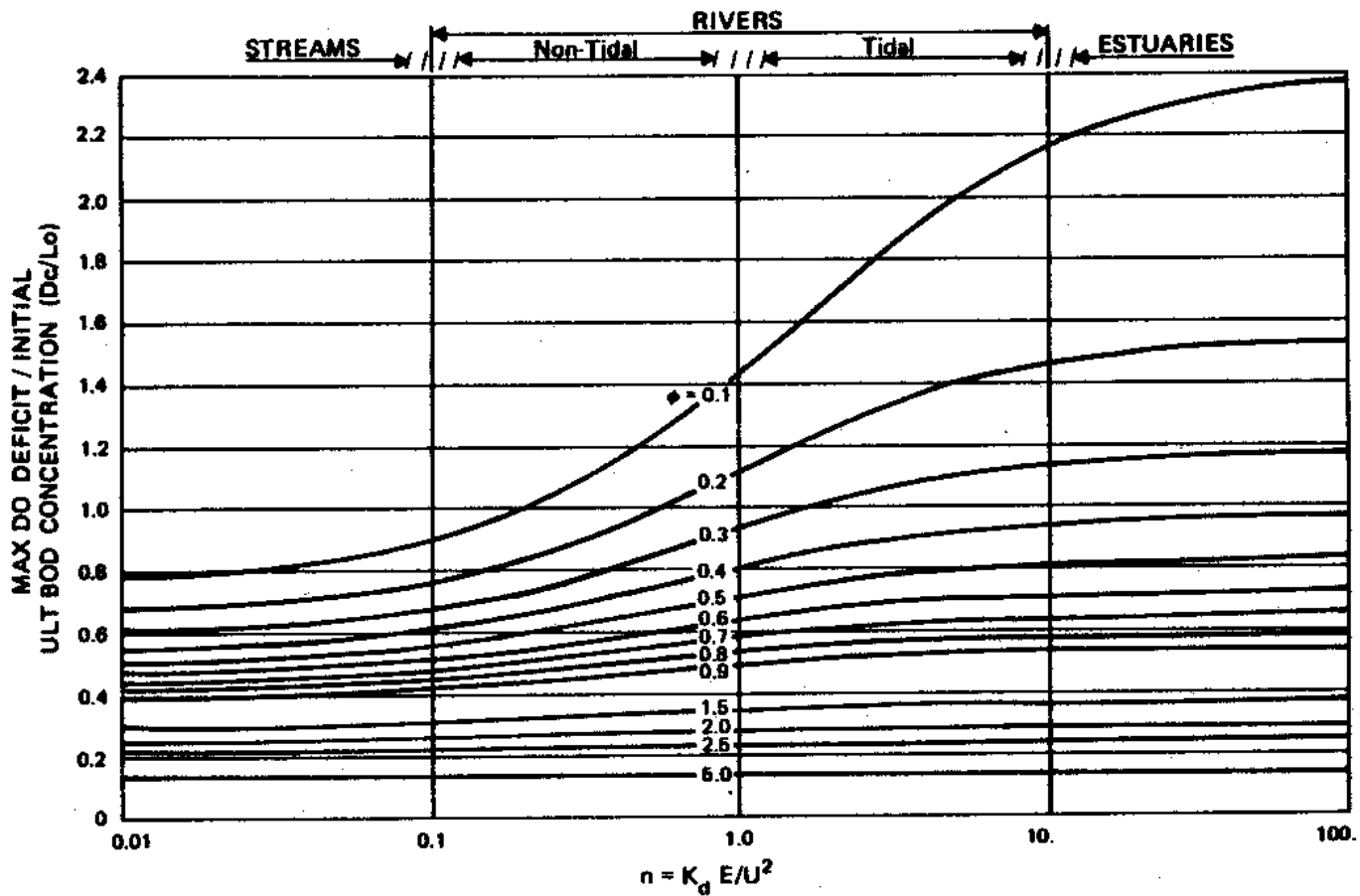


Figure 3-0. Dissolved oxygen response as a function of $K_d E/U^2$.

Figure prepared by O'Connor

From: Technical Guidance Manual for Performing Waste Load Allocations: Book II, Chapter 1

Full Equation

$$D = D_o e^{-k_a t} + \frac{k_d L_o}{k_a - k_r} (e^{-k_r t} - e^{-k_a t})$$

$$+ \frac{k_n L_{No}}{k_a - k_n} (e^{-k_n t} - e^{-k_a t})$$

Point NBOD

$$+ \frac{-P + R + \left(\frac{S'_B}{H} \right)}{k_a} (1 - e^{-k_a t})$$

$$+ \frac{k_d S_d}{k_r k_a} (1 - e^{-k_a t}) - \frac{k_d S_d}{k_r (k_a - k_r)} (e^{-k_r t} - e^{-k_a t})$$

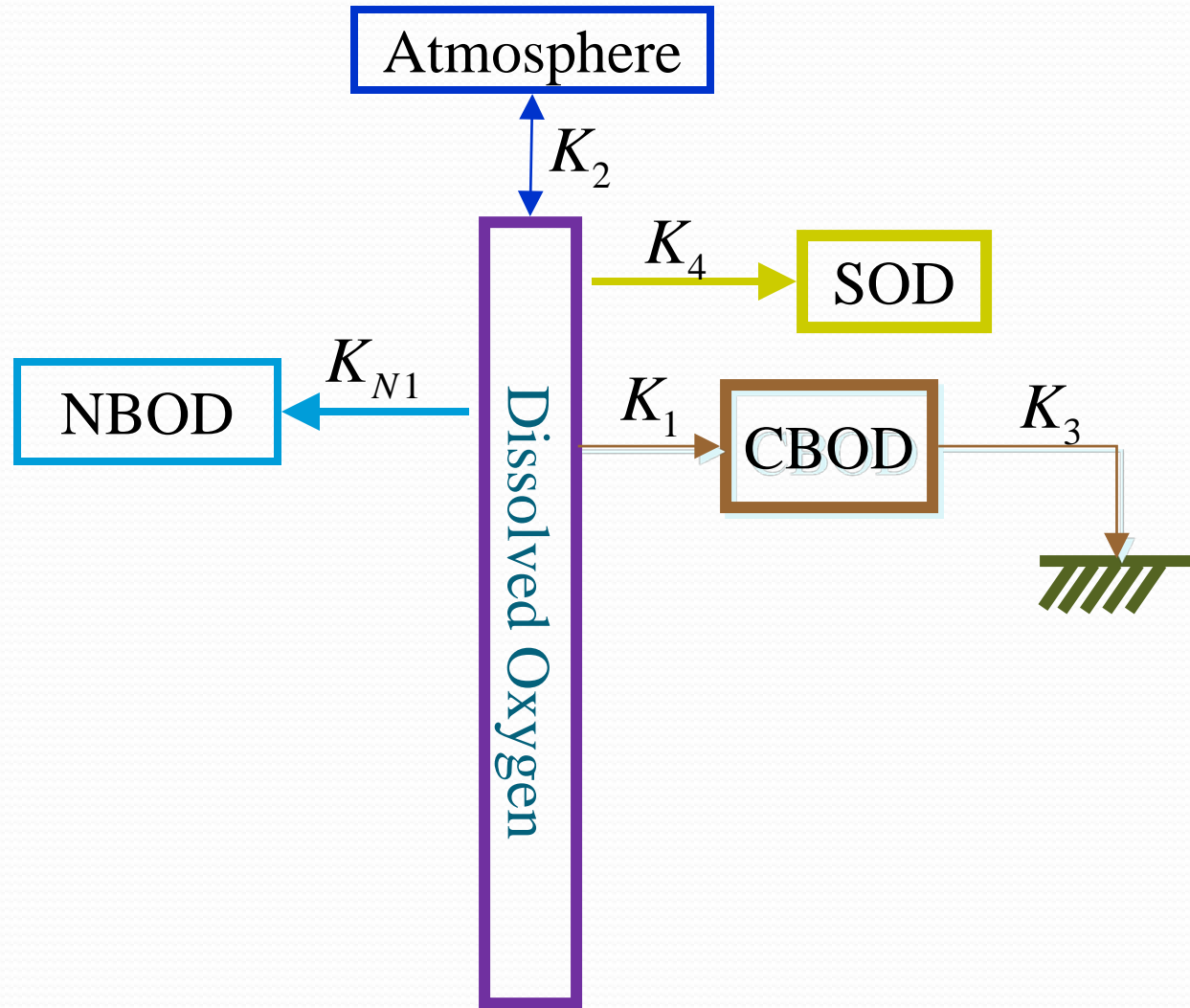
$$+ \frac{k_n S_{Nd}}{k_n k_a} (1 - e^{-k_a t}) - \frac{k_n S_{Nd}}{k_n (k_a - k_n)} (e^{-k_n t} - e^{-k_a t})$$

Distributed NBOD

Additional notes on WLA (cont.)

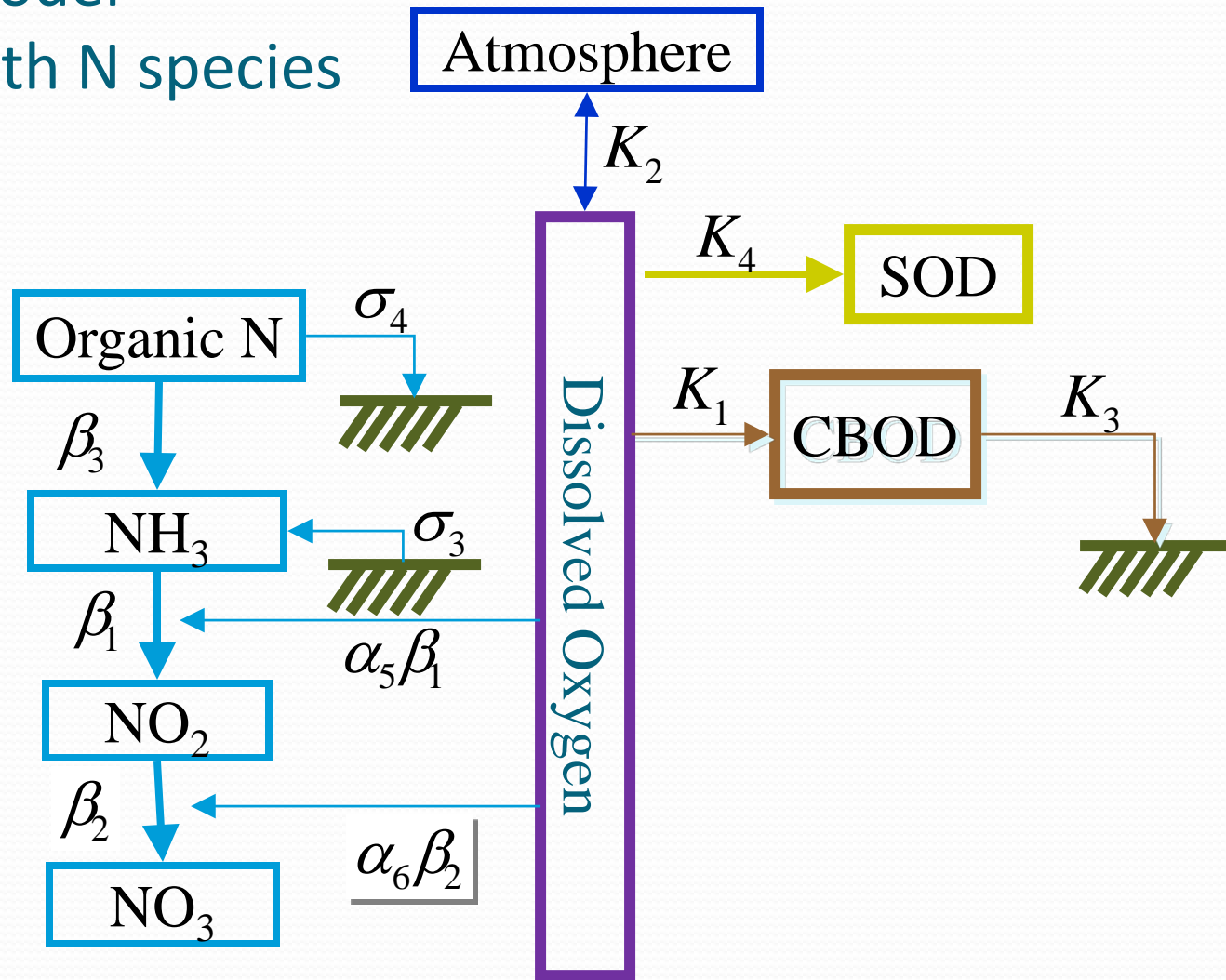
- Nitrogen modeling
 - NBOD
 - measure and model TKN only
 - all 4 major species
 - org-N, NH_3 , NO_2 , and NO_3
 - requires separate analysis of loadings, rate coefficients, etc.

General Model Kinetics



General Model

Kinetics with N species

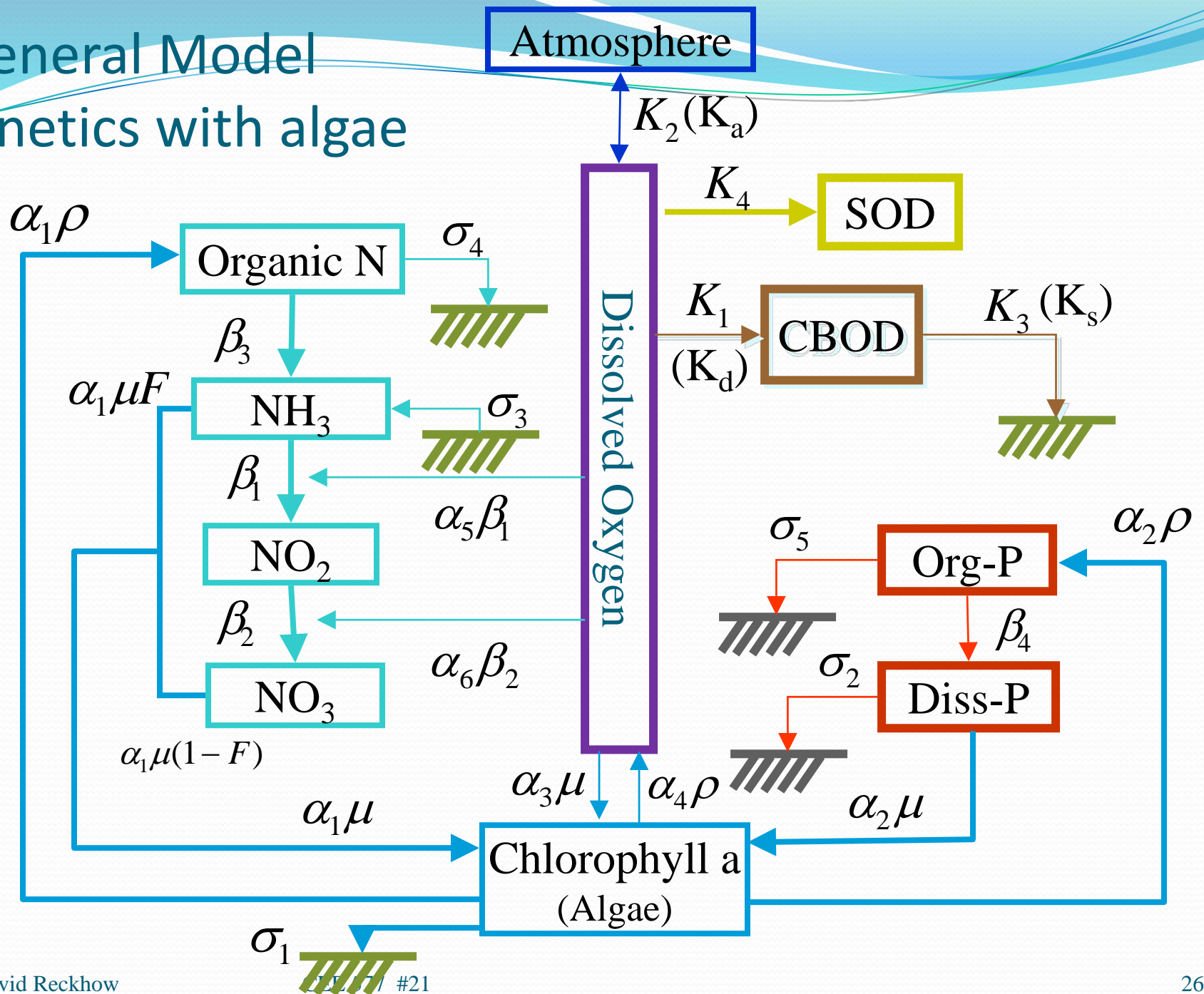


Additional notes on WLA (cont.)

- Algal modeling
 - Level I
 - measure P-R: diurnal swings in D.O.
 - Level II
 - measure chlorophyll a, light, light extinction, nutrients “in-situ”
 - calculate P-R
 - Level III
 - assess nutrient loadings, light extinction
 - model nutrient conc., chlorophyll a, P-R

General Model

Kinetics with algae



- To next lecture

- Ohio River

