

Homework #6**Toxics Models**

4 points total
for entire
homework

1. Problem 40.1

Thomann and DiToro (1983) presented the following data related to the solids budget for the Western Basin of Lake Erie:

$$\begin{array}{ll} \text{Volume} = 23 \times 10^9 \text{ m}^3 & \text{Area} = 3030 \times 10^6 \text{ m}^2 \\ \text{Solid loading} = 11.4 \times 10^{12} \text{ g/yr} & \text{Suspended Solids} = 20 \text{ mg/L} \\ \text{Flow} = 167 \times 10^9 \text{ m}^3/\text{yr} & \end{array}$$

They assumed that the solids settle at a rate of 2.5 m/d (912.5 m/yr), and that the sediments have $\rho = 2.4 \text{ g/mL}$ and $\phi = 0.9$. Determine the burial and resuspension velocities.

Solution:

1 point for
#1

First, an inflow concentration can be determined as

$$\begin{aligned} m_{in} &= \frac{W_{solids}}{Q} = \frac{Qm_{in}}{Q} \\ m_{in} &= \frac{11.4 \times 10^{12}}{167 \times 10^9} = 68.26 \frac{\text{mg}}{\text{L}} \end{aligned}$$

Next, equation 40.25 can be used to calculate:

$$\begin{aligned} v_b &= \frac{Q(m_{in} - m)}{A(1 - \phi)\rho} \\ v_b &= \frac{167 \times 10^9}{3030 \times 10^6} \frac{68.26 - 20}{(1 - 0.9)2.4 \times 10^6} \\ &= 0.0111 \frac{\text{m}}{\text{yr}} \\ &= 11.1 \frac{\text{mm}}{\text{yr}} \end{aligned}$$

This result can be substituted into equation 40.26 to determine:

$$v_r = v_s \frac{m}{(1 - \phi)\rho} - v_b$$

$$\begin{aligned}
 v_r &= 912.5 \frac{20}{(1-0.9)24 \times 10^6} - 0.0111 \\
 &= 0.06494 \frac{m}{yr} \\
 &= 64.94 \frac{mm}{yr}
 \end{aligned}$$

2. Problem 40.2

Suppose that a toxic substance that is subject to volatilization ($v_v = 100$ m/yr) is discharged to Lake Huron with an inflow concentration of $100 \mu\text{g/L}$. In the absence of sediment feedback, determine the concentration for three cases: (a) weak sorber ($K_d = 0.002 \text{ m}^3/\text{g}$), (b) moderate sorber ($K_d = 0.1$), and (c) strong sorber ($K_d = 2$). Other necessary information should be taken from Examples 40.1 and 40.2.

Solution:

a. for the weak sorber

The fraction in dissolved form is:

$$\begin{aligned}
 F_d &= \frac{1}{1 + K_d m} \\
 F_d &= \frac{1}{1 + 0.002(0.531)} = 0.9989
 \end{aligned}$$

and

$$F_p = 1 - F_d = 0.0011$$

Thus, the steady-state concentration can be calculated from equation 40.11 as:

$$\begin{aligned}
 c &= \frac{Qc_{in}}{Q + kV + v_v AF_d + v_s AF_p} \\
 &= \frac{1.61 \times 10^{11} (100 \mu\text{g} / L)}{1.61 \times 10^{11} + 100(5.96 \times 10^{10})0.9989 + 191.82(5.96 \times 10^{10})0.0011} \\
 &= 2.63 \mu\text{g} / L
 \end{aligned}$$

Note that I used the lower value for v_s from example problems 40.1 and 40.2. The reason is that this value was determined based on a model without sediment feedback (e.g., resuspension) much like the problem we're doing.

b. for the moderate sorber

The fraction in dissolved form is determined to be 0.9496

Thus, the steady-state concentration can be calculated from equation 40.11 as:

1.5 points
for #2

$$\begin{aligned}
 c &= \frac{Qc_{in}}{Q + kV + v_v AF_d + v_s AF_p} \\
 &= \frac{1.61 \times 10^{11} (100 \mu\text{g} / \text{L})}{1.61 \times 10^{11} + 100(5.96 \times 10^{10})0.9496 + 191.82(5.96 \times 10^{10})0.0504} \\
 &= 2.52 \mu\text{g} / \text{L}
 \end{aligned}$$

c. for the strong sorber

The fraction in dissolved form is determined to be 0.485

Thus, the steady-state concentration can be calculated from equation 40.11 as:

$$\begin{aligned}
 c &= \frac{Qc_{in}}{Q + kV + v_v AF_d + v_s AF_p} \\
 &= \frac{1.61 \times 10^{11} (100 \mu\text{g} / \text{L})}{1.61 \times 10^{11} + 100(5.96 \times 10^{10})0.485 + 191.82(5.96 \times 10^{10})0.515} \\
 &= 1.80 \mu\text{g} / \text{L}
 \end{aligned}$$

3. Problem 40.3a

A substance ($K_d = 0.02 \text{ m}^3/\text{d}$; $M = 300$) is discharged into a lake ($c_{in} = 100 \mu\text{g}/\text{L}$) having the following characteristics:

Volume = $1 \times 10^6 \text{ m}^3$	Mean depth = 5 m
Residence time = 1 year	Suspended solids = 10 mg/L
Settling velocity = 50 m/yr	Sediment deposition = $100 \text{ g}/\text{m}^3/\text{yr}$
Sediment porosity = 0.85	Sediment density = $2.5 \text{ g}/\text{cm}^3$

- (a) If the resuspension is negligible, compute the steady-state concentration for three levels of volatilization:
- high soluble ($v_v = 0$)
 - moderately soluble ($v_v = 10 \text{ m}/\text{yr}$)
 - nearly insoluble ($v_v = 100 \text{ m}/\text{yr}$)

Solution

The fractions in the dissolved and particulate form can be determined from:

$$F_d = \frac{1}{1 + 0.02(10)} = 0.8333$$

and

$$F_p = 1 - F_d = 0.1667$$

1.5 points
for #2

i. highly soluble

The concentration in the water can be calculated as:

$$\begin{aligned}
 c &= \frac{Qc_{in}}{Q + kV + v_v AF_d + v_s AF_p} \\
 &= \frac{10^6 (100 \mu\text{g} / L)}{10^6 + 0 \left(\frac{10^6}{5} \right) 0.8333 + 50 \left(\frac{10^6}{5} \right) 0.1667} \\
 &= 37.5 \mu\text{g} / L
 \end{aligned}$$

ii. moderately soluble

The concentration in the water can be calculated as:

$$\begin{aligned}
 c &= \frac{Qc_{in}}{Q + kV + v_v AF_d + v_s AF_p} \\
 &= \frac{10^6 (100 \mu\text{g} / L)}{10^6 + 10 \left(\frac{10^6}{5} \right) 0.8333 + 50 \left(\frac{10^6}{5} \right) 0.1667} \\
 &= 23.08 \mu\text{g} / L
 \end{aligned}$$

iii. insoluble

The concentration in the water can be calculated as:

$$\begin{aligned}
 c &= \frac{Qc_{in}}{Q + kV + v_v AF_d + v_s AF_p} \\
 &= \frac{10^6 (100 \mu\text{g} / L)}{10^6 + 100 \left(\frac{10^6}{5} \right) 0.8333 + 50 \left(\frac{10^6}{5} \right) 0.1667} \\
 &= 5.17 \mu\text{g} / L
 \end{aligned}$$