Process Kinetics

Lab Lecture the week of Oct 19 Lab held in Marston 10 the week of Oct 26



- Develop a kinetic rate equation for the destruction of Naproxen with aqueous chlorine
- Use the rate equation to assess relative costs of a water and wastewater treatment to inform process design
 - Naproxen: a synthetic compound used as an antiinflammatory drug, especially in the treatment of headache and arthritis

What is Kinetics?

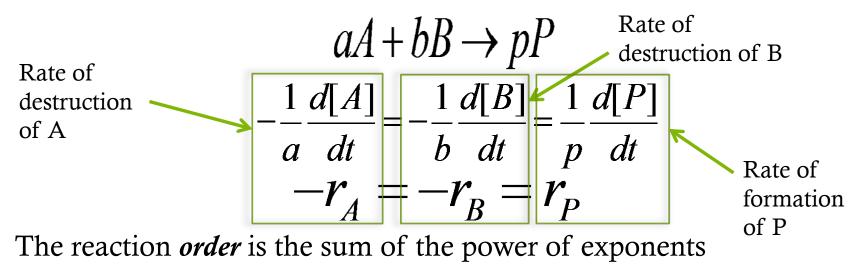
- The study of :
- 1. the *speed* with which a chemical reaction occurs: *the rate at which the concentrations of reactants and products change*

and,

- 2. the *factors* that affect this speed
 - Concentration
 - Temperature
 - Phase (solid, liquid, or gas)
 - Surface area
 - Solvent
 - Presence/absence of a catalyst



• The rate of formation or consumption of a compound (r)



 $r = d[A]/dt = -k[A]^a[B]^b$

k - reaction rate constant; dependent on temperature and pressure

Summary of Reaction Kinetics

| Order | Reaction | Rate Equation | Integrated Form (A=A ₀ at t=0) | Half-Life (t for [A]=0.5 A ₀] |
|-------|----------------|---------------------|------------------------------------------------------------------------------------|-------------------------------------------------|
| 0 | A→ B | d[A]/dt = -k | $[A] = A_0 - kt$ | A ₀ /2k |
| 1 | A→ B | d[A]/dt = -k[A] | $[A] = A_0 e^{-kt}$ | 0.693/k |
| 2 | A+A → B | $d[A]/dt = -k[A]^2$ | $1/[A]=1/A_0 + kt$ | 1/kA ₀ |
| | A+B → P | d[A]/dt = -k[A][B] | $ln ([B]/[A]) = ln(B_0/A_0) + (B_0-A_0)kt$ (for A_0 \neq B_0, [B] = B_0 at t=0) | |
| | | | 1 T 1 (0010) | |

From Benjamin and Lawler (2012)

Determining Order of Reaction by Method Integration

| Plotting Procedure to Determine Order of Reaction by Method of Integration | | | | | |
|----------------------------------------------------------------------------|---------------------|------------------------|-------------|-------|--|
| Order | Rate Equation | Integrated Equation | Linear Plot | Slope | |
| 0 | d[A]/dt = -k | $[A] - [A]_0 = -kt$ | [A] vs. 1 | -k | |
| 1 | d[A]/dt = -k[A] | $\ln[A]/[A]_0 = -kt$ | In[A] vs. J | -k | |
| 2 . | $d[A]/dt = -k[A]^2$ | $1/[A] - 1/[A]_0 = kt$ | 1/[A] vs. † | k | |

Source: Henry and Heinke, 1989. Reprinted with permission.

Chlorine as a Disinfectant

- Used in both water treatment and wastewater treatment to disinfect and deactivate germs
- Very strong oxidant and will inactivate microorganisms and also react with other water constituents
- Three forms of chlorine in water treatment
 - Free: chlorine composed of dissolved hypochlorite ions, hypochlorous acid, and chlorine gas
 - Combined: chlorine in water combined with ammonia to form chloramines
 - Total: sum of free and combined chlorine
- Efficacy:
 - HOCl>OCl->inorganic chloramines>organic chloramines

Residual Chlorine

• The amount of chlorine that remains in the water after a certain period of contact time

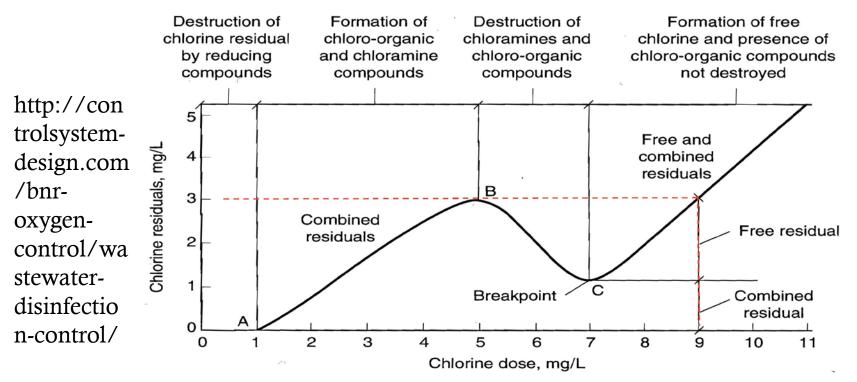
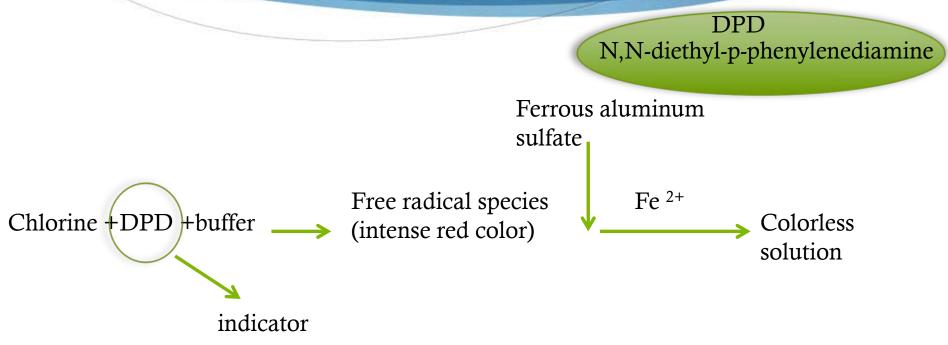


Figure 1: Breakpoint chlorination curve

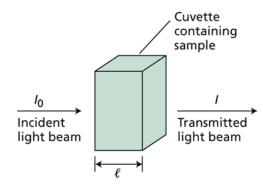
To measure residual chlorine concentration



- No. of mLs titrant used = chlorine residual in mg/L Cl_2
- (back calculate to original sample conc. using dilution factor).

To measure UV absorbance

- A UV-Vis Spectrophotometer will be used
- Basic theory of molecular absorption spectroscopy is basied on the measurement of the absorbance A (or transmittance T) of solution contained in a transparent cell with a path length 1 (Skoog et al., 2007).



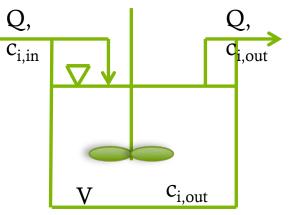
• Beer's Law: The concentration of the absorbing analyte is linearly related to t $A = -\log T = \log \frac{l_0}{r} = \varepsilon lc$

 I_0 is radiant power in watts incident on sample; I is radiant power transmitted by sample; ϵ is molar absorptivity (M⁻¹cm⁻¹); 1 is length over which attenuation occurs (usually 1 cm, which is what we'll be using); c is concentration in specified units (usually in M)

Useful Information CFSTR

 Continuous flow stirred tank reactor (CFSTR) at steady state:

$$V \frac{dc_{i,out}}{dt} = Q(c_{i,in} - c_{i,out}) + Vr$$
$$0 = Q(c_{in} - c_{out}) + Vr_i$$
$$\tau = V / Q$$
$$\tau_{CFSTR} = -\frac{C_{in} - C_{out}}{r_{c_{out}}}$$

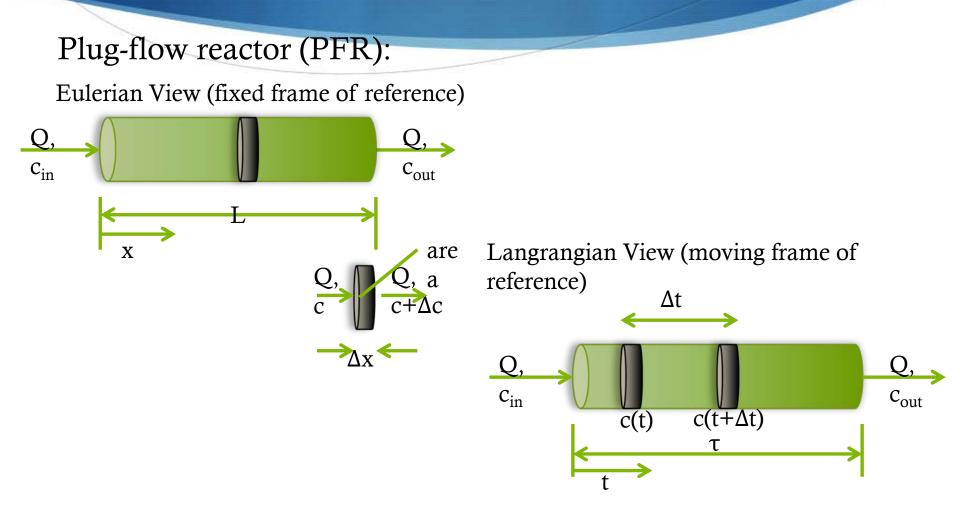


Useful Information CFSTR

| Reaction order, n (r=-k _n c ⁿ) | C _{out} | C _{out} /C _{in} | τ _{pfr} |
|----------------------------------------------------------|-----------------------------|-----------------------------------|----------------------------------------------|
| 0 | c_{in} - $k_0 \tau$ | 1- $(k_0 \tau / c_{in})$ | $1/k_0 *$ (c_{in}/c_{out}) |
| 1 | $c_{in}exp(-k_1\tau)$ | exp(-k ₁ τ) | $1/k_1 * \ln (c_{in}/c_{out})$ |
| 2 | $c_{in}/(1+k_2\tau c_{in})$ | $1/(1+k_2\tau c_{in})$ | $1/k_2 c_{in}^*$ ((c_{in}/c_{out})-1) |

From Benjamin and Lawler (2012)

Useful Information PFR



Useful information PFR

| Reaction order | C _{out} | C _{out} /C _{in} | $	au_{PFR}$ |
|----------------|-----------------------|-----------------------------------|----------------------------------------------------|
| 0 | c_{in} - $k_0 \tau$ | 1- $(k_0 \tau / c_{in})$ | $\frac{C_{out}/k_0 *}{((c_{in}/c_{out})-1)}$ |
| 1 | $c_{in}/(1+k_1\tau)$ | $1/(1+k_1\tau)$ | $1/k_1 *$ ((c_{in}/c_{out})-1) |
| 2 | | $1/(1+k_2\tau c_{out})$ | $\frac{1/k_2 c_{out}^*}{((c_{in}^*/c_{out}^*)-1)}$ |

From Benjamin and Lawler (2012)

Comparison of CFSTRs and PFRs

- For first and second order reactions, more detention time is required in a CFSTR than a PFR to accomplish the same amount of removal.
- For a zero-order reaction, the two systems perform identically
- Why use CFSTRs?
 - Water and wastewater treatment equalization basins
 - Mixing of chemicals
 - Less dead space and short circuiting